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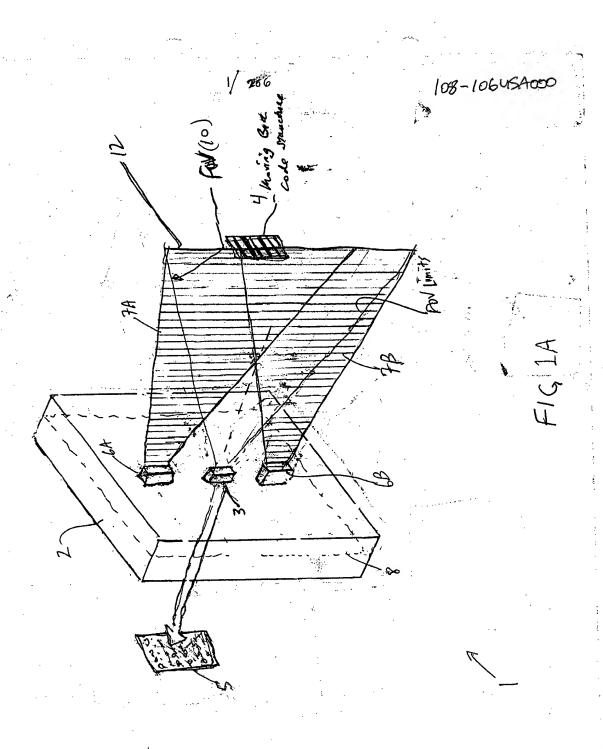
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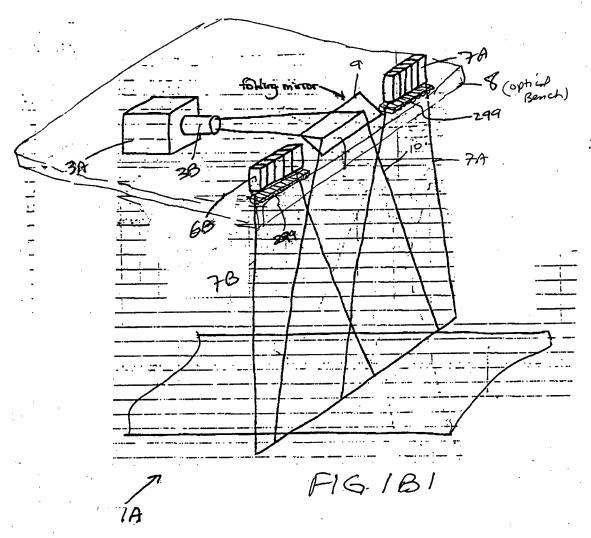
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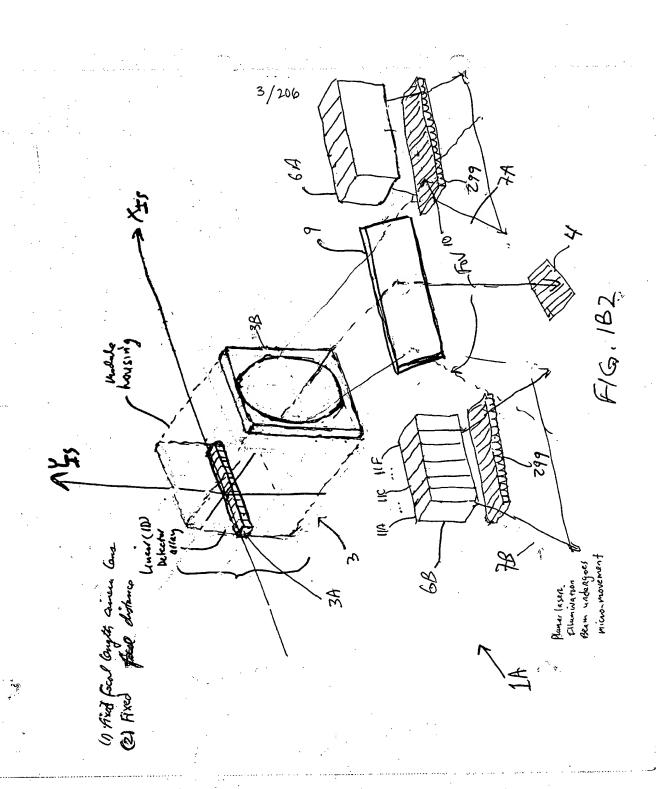
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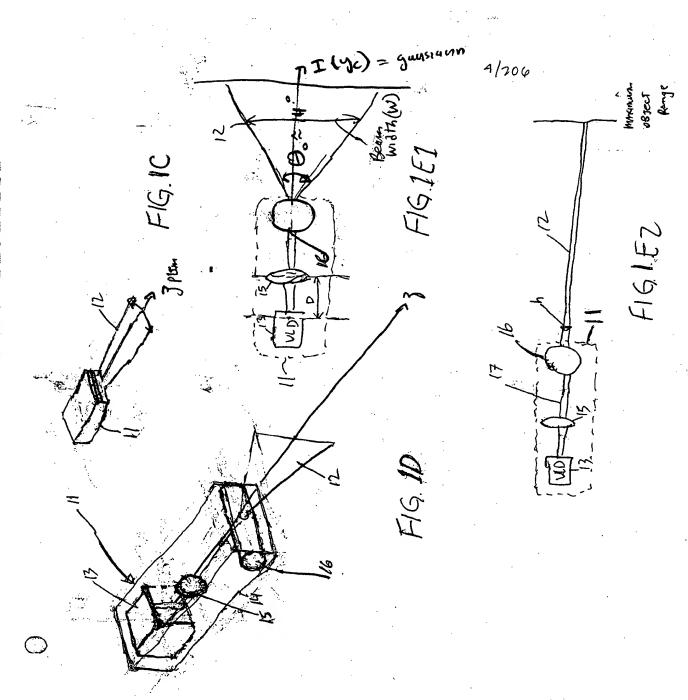
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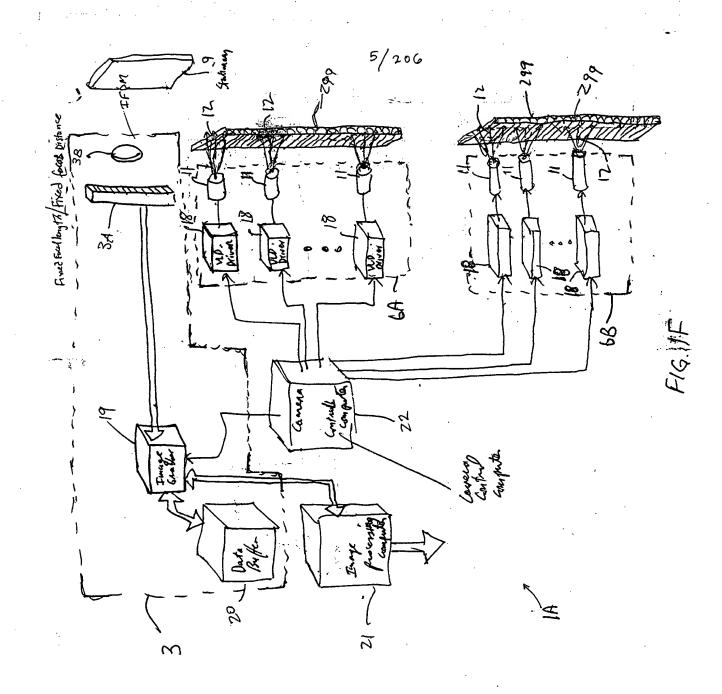


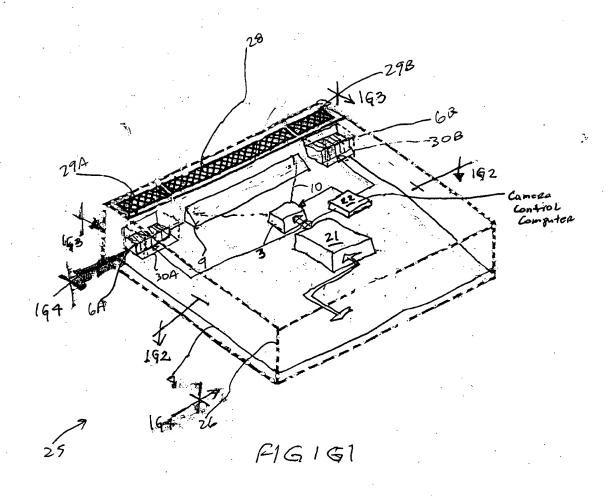


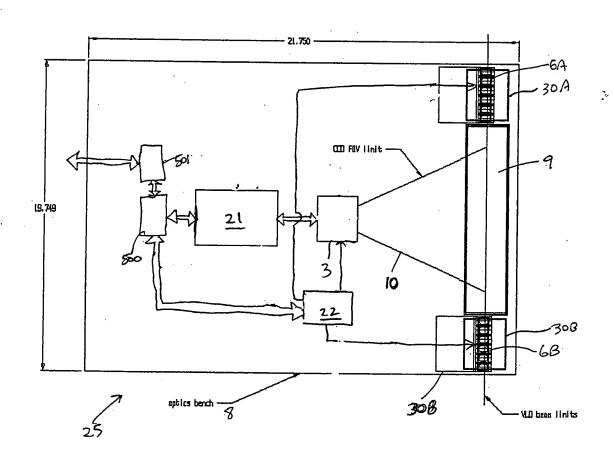




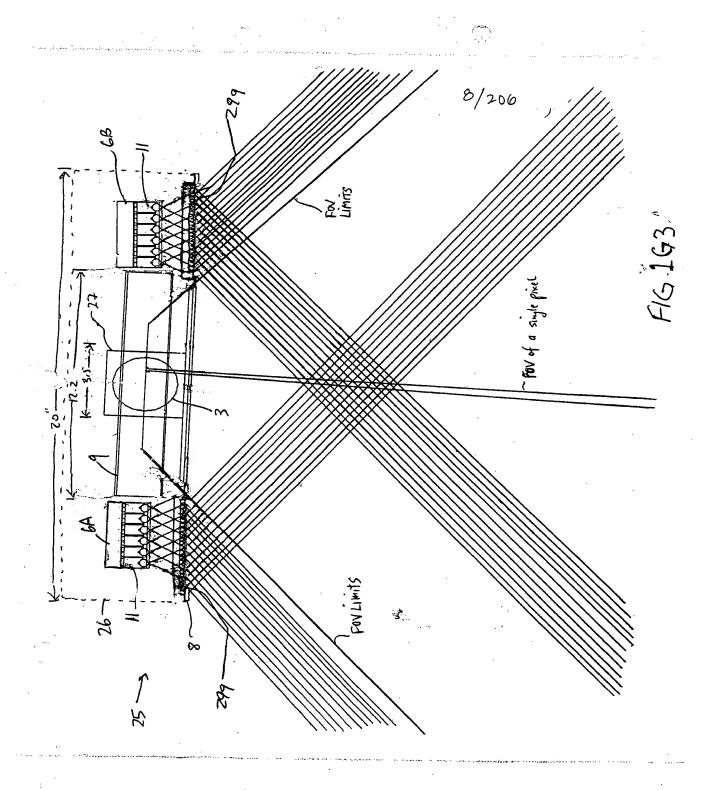








F16. 162



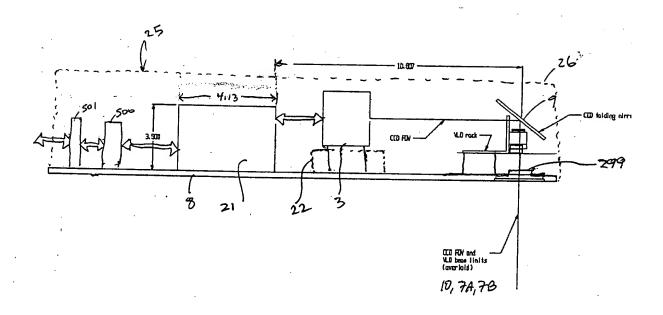
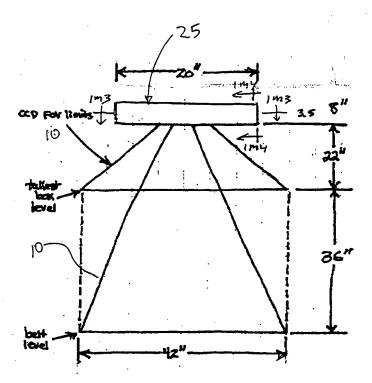


FIG. 164.





& Fixed Field of Field

F16. 165



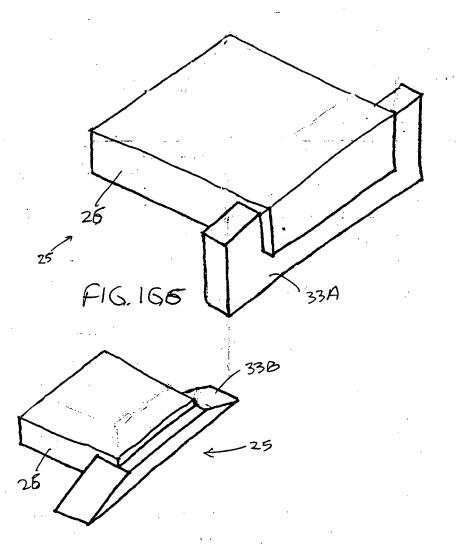
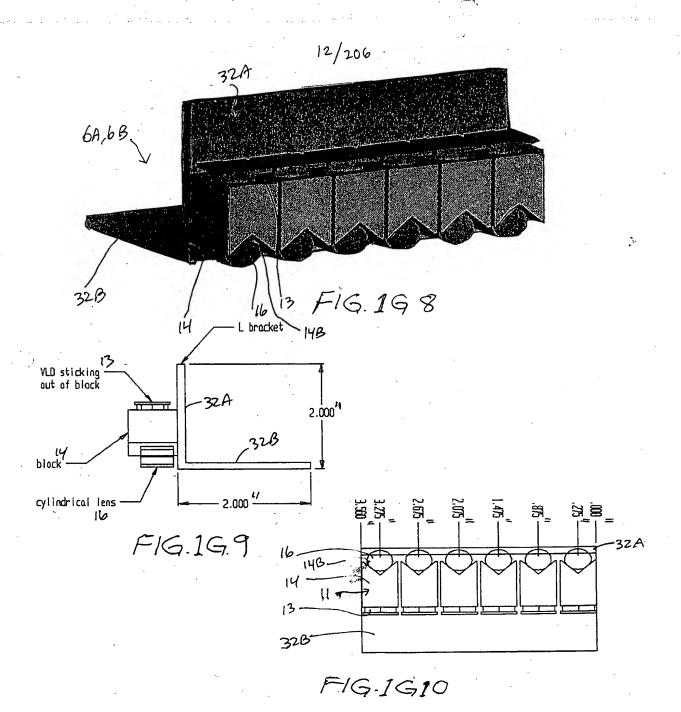
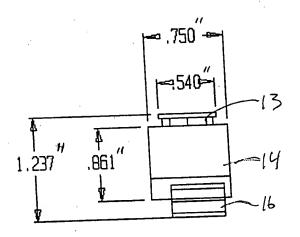


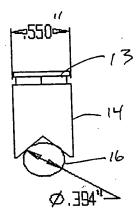
FIG.1G7







F16.1611



F16-1612

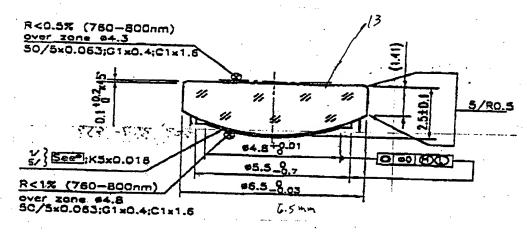


FIG. 1913

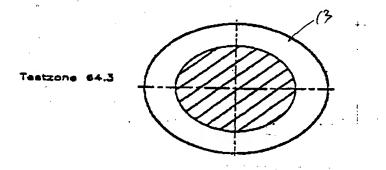


FIG. 1G14

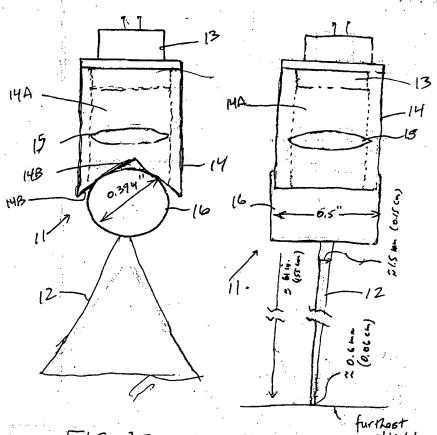
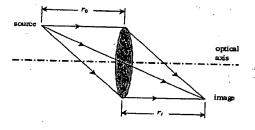


FIG 1G15A FIG. 1G15B distance

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F16-141

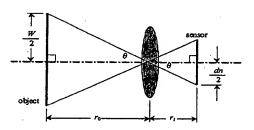
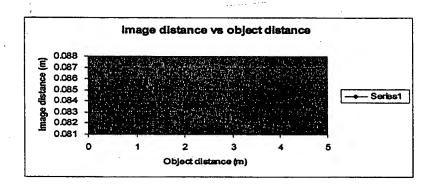
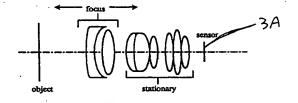


FIG. 1HZ

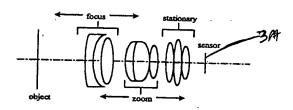
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F/G. 1H3



F16. 1H4



F16 1H5

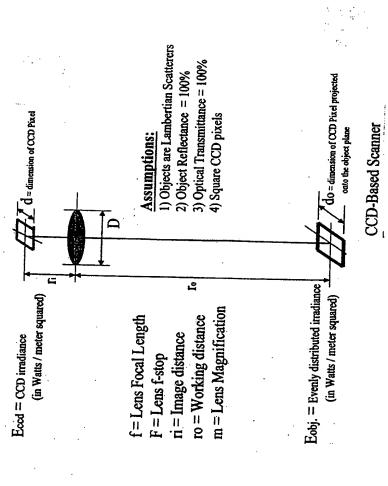


FIG 146

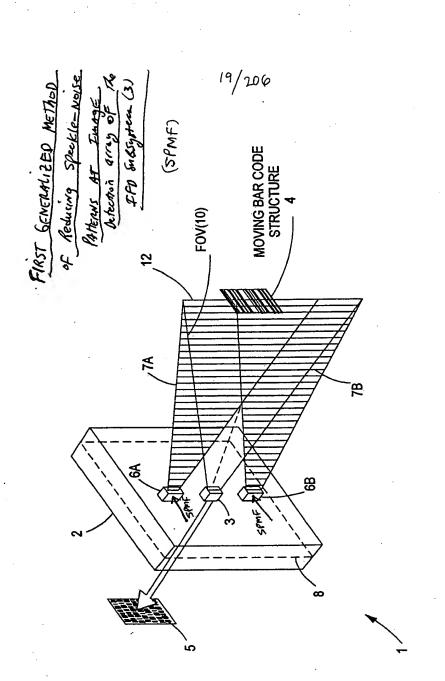


FIG. (II

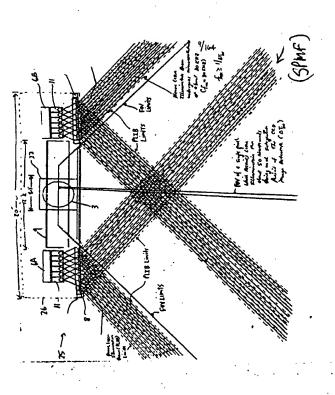


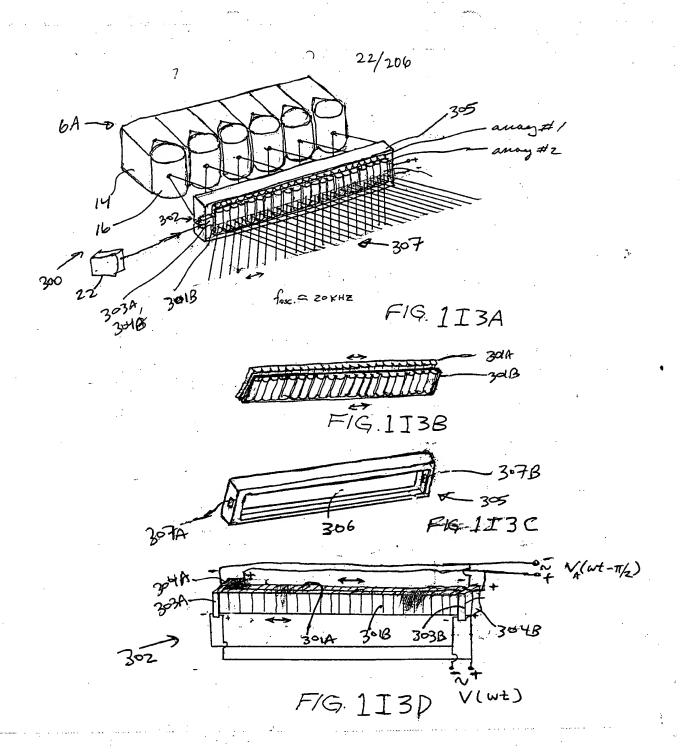
FIG. II :ZA Rim to object Islumoration

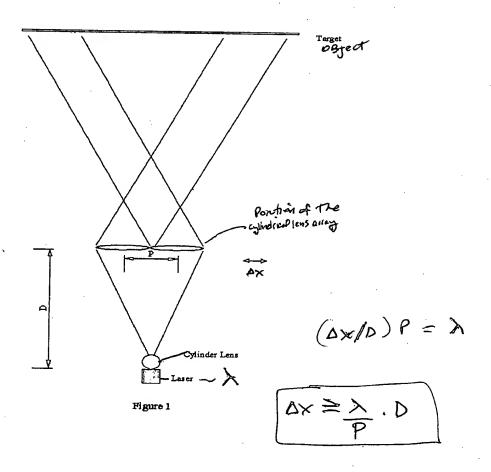
The First Generalized Speckle-Noise Pattern Reduction Method Of The Present Invention

Prior to illumination of the target with the planar laser illumination beam (PLIB), modulate the spatial phase of the transmitted PLIB along the planar extent thereof according to a spatial phase modulation function (SPMF) so as to modulate the phase along the wavefront of the transmitted PLIB and produce numerous substantially different time-varying speckle-noise patterns at the image detection array of the IFD Subsystem during the photo-integration time period thereof.

Temporally average the numerous substantially different time-varying speckle-noise patterns produced at the image detection array in the IFD Subsystem during the photo-integration time period thereof, so as to thereby reduce the power of the speckle-noise pattern observed at the image detection array.

FIG. 1IZB





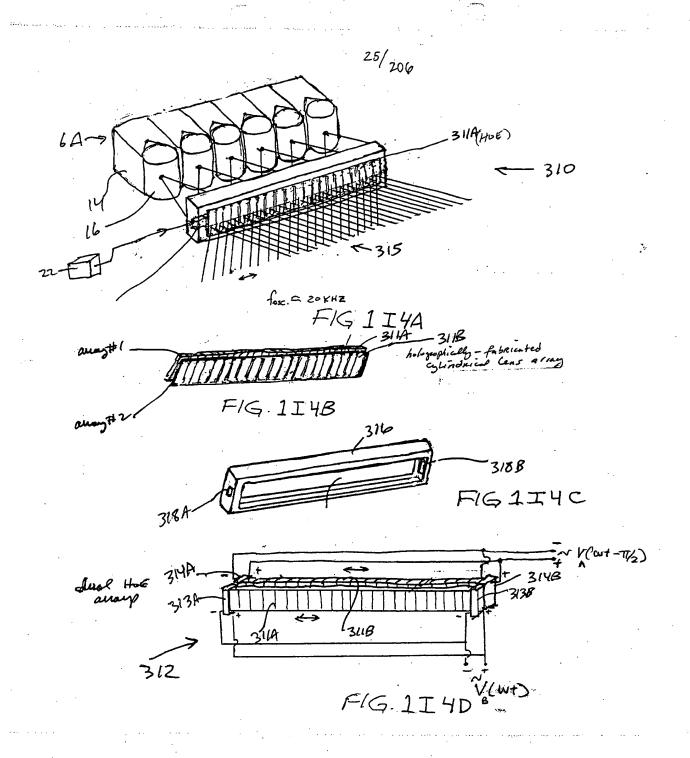
F/G. 1I3E

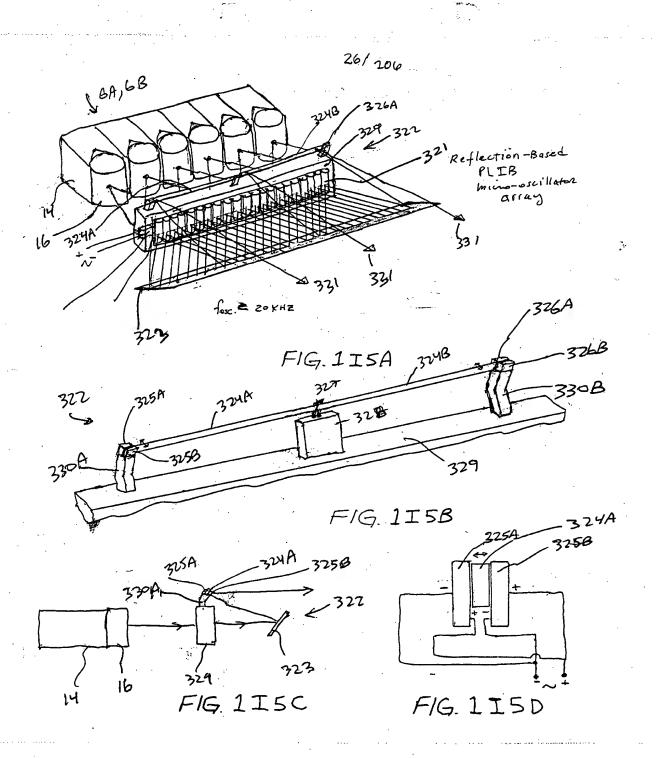


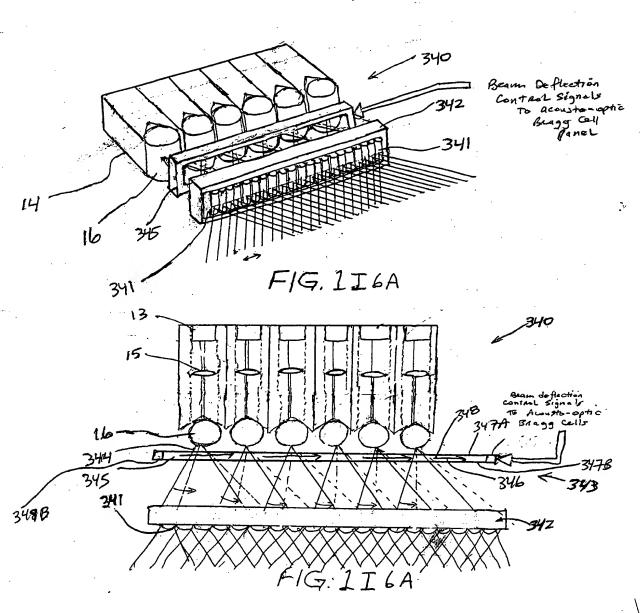
F19.1I3F



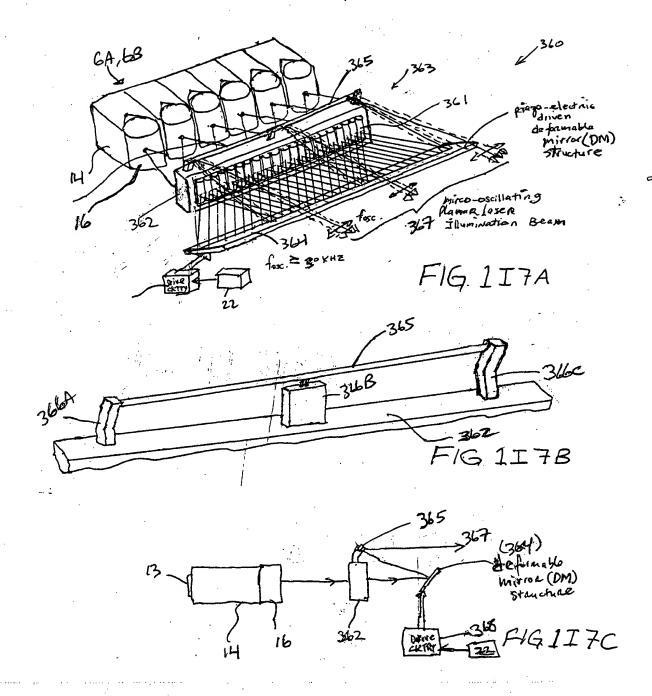
F1G 1I36

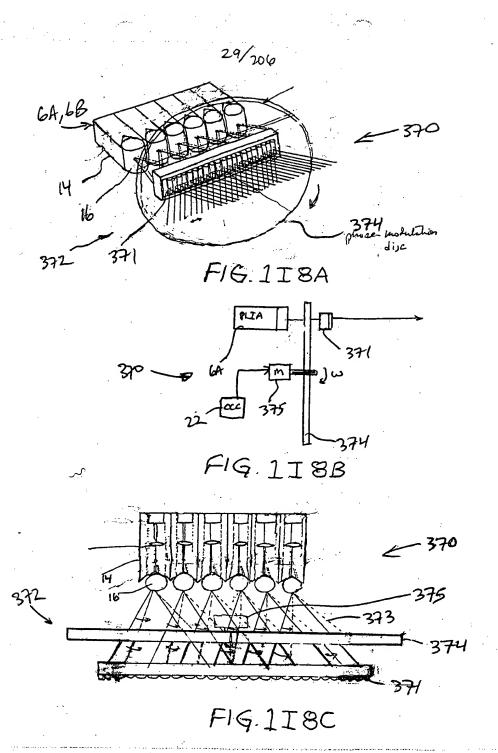




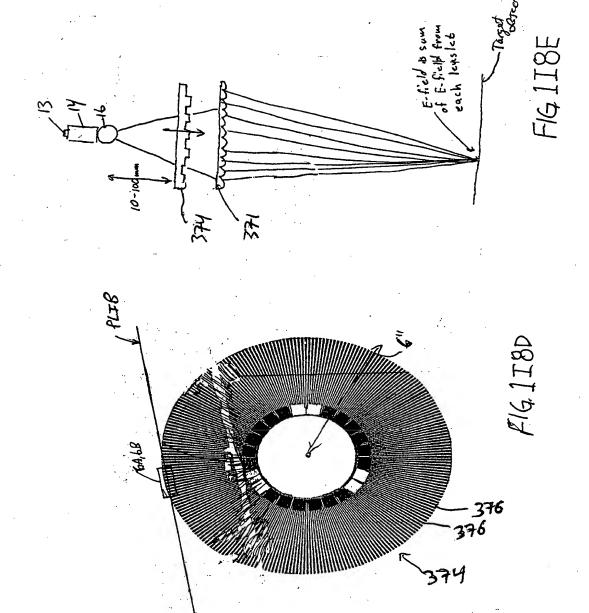


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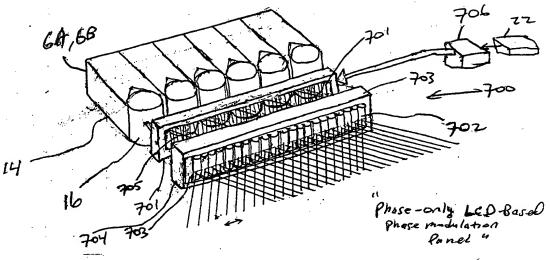


FIG.118F

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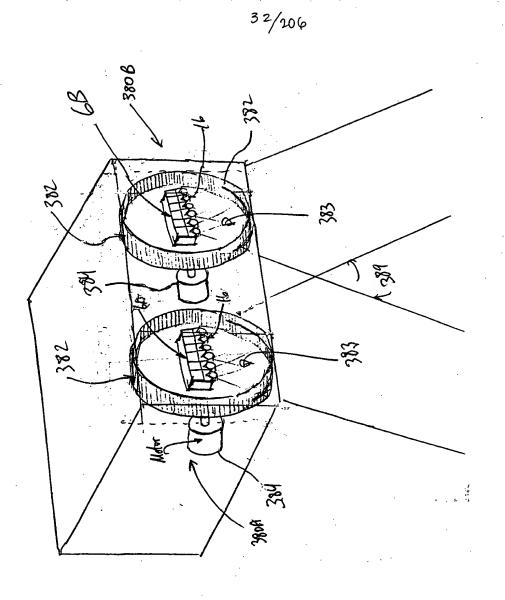
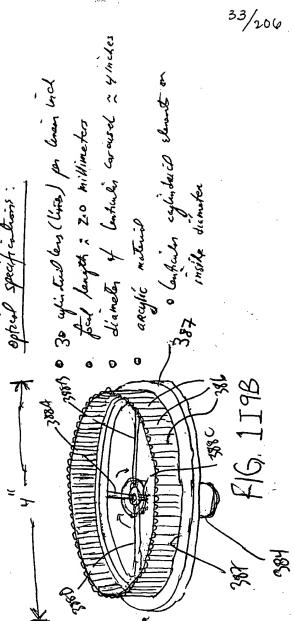
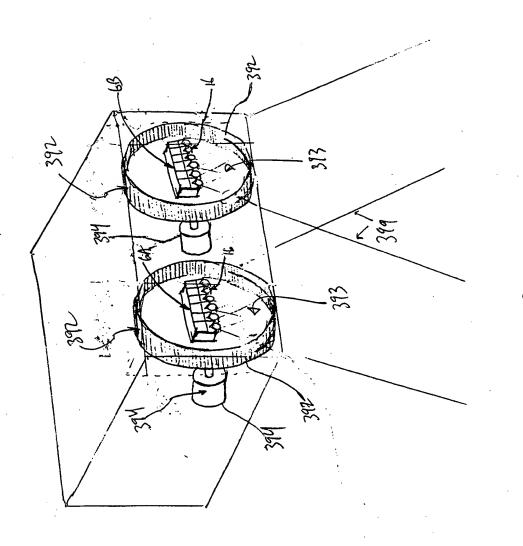


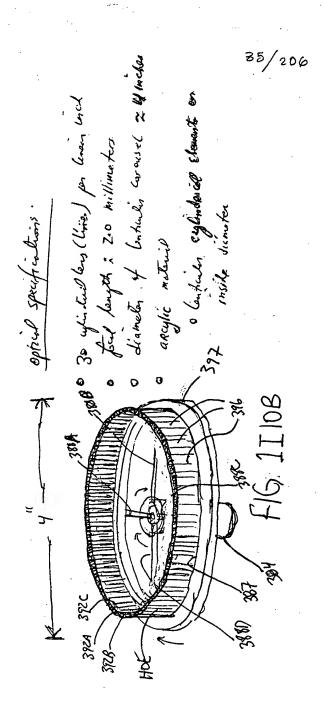
FIG. II TA



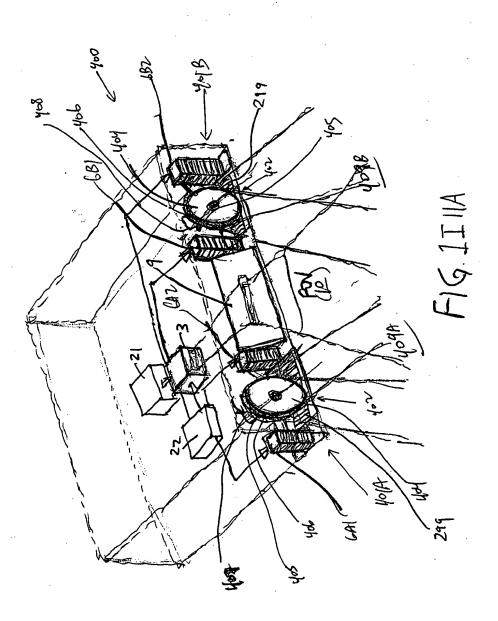
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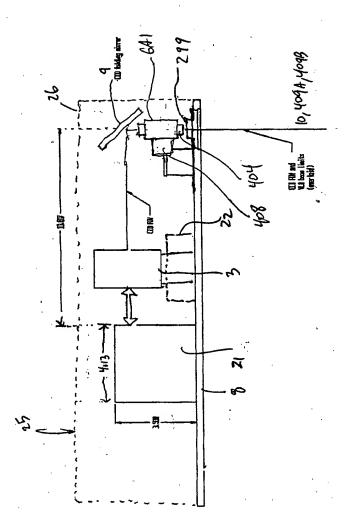


16 11 10A

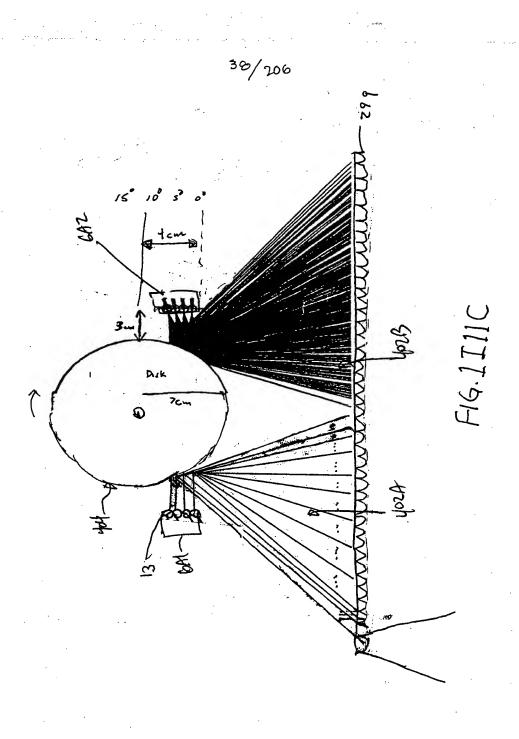


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HG 11118

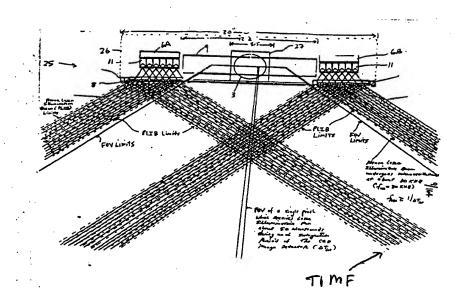


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F16. 1 I 13A

The Second Generalized Speckle-Noise Pattern Reduction Method Of The Present Invention

Prior to illumination of the target with the planar laser illumination beam (PLIB), modulate the temporal intensity of the transmitted PLIB along the planar extent thereof according to a temporal intensity modulation function (TIMF) so as to modulate the phase along the wavefront of the transmitted PLIB and produce numerous substantially different time-varying specklenoise patterns at the image detection array of the IFD Subsystem during the photo-integration time period thereof.

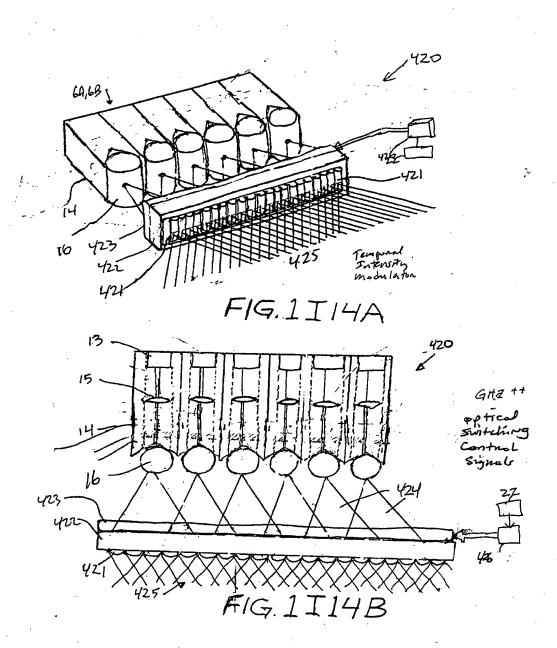
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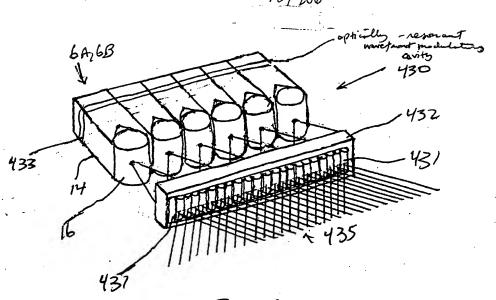
Temporally average the numerous substantially different time-varying speckle-noise patterns produced at the image detection array in the IFD Subsystem during the photo-integration time period thereof, so as to thereby reduce power of the speckle-noise pattern observed at the image detection

array.

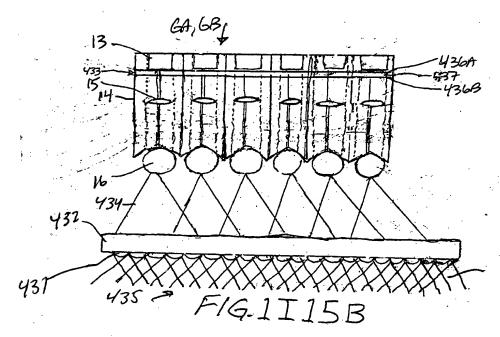
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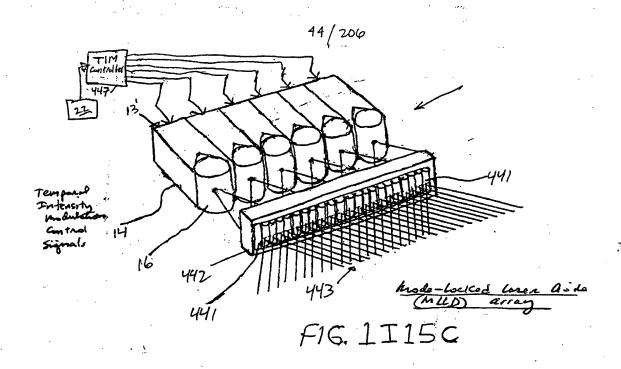
FIG 1113B





F16. 1I15A





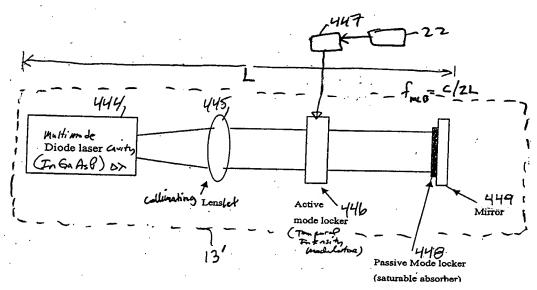
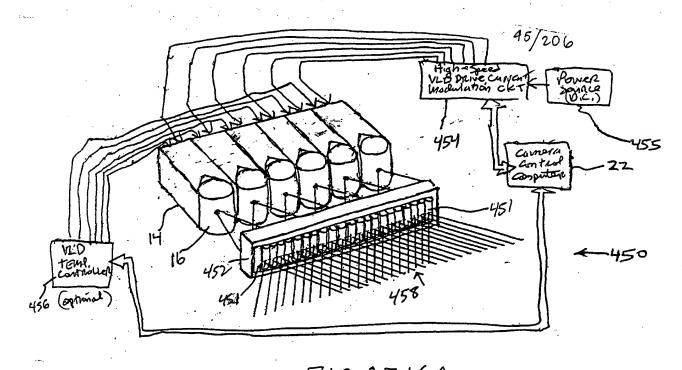
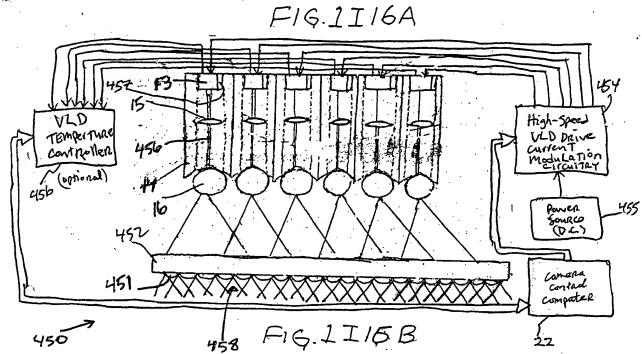


FIG.1I15D





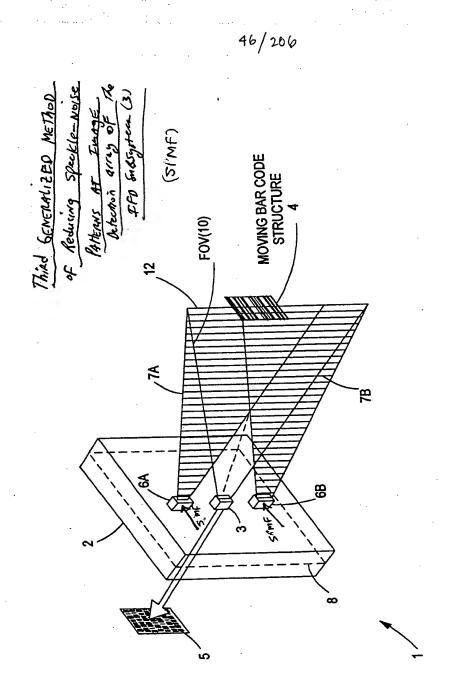
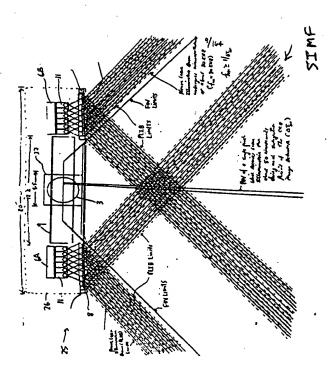


FIG. 1I 18A

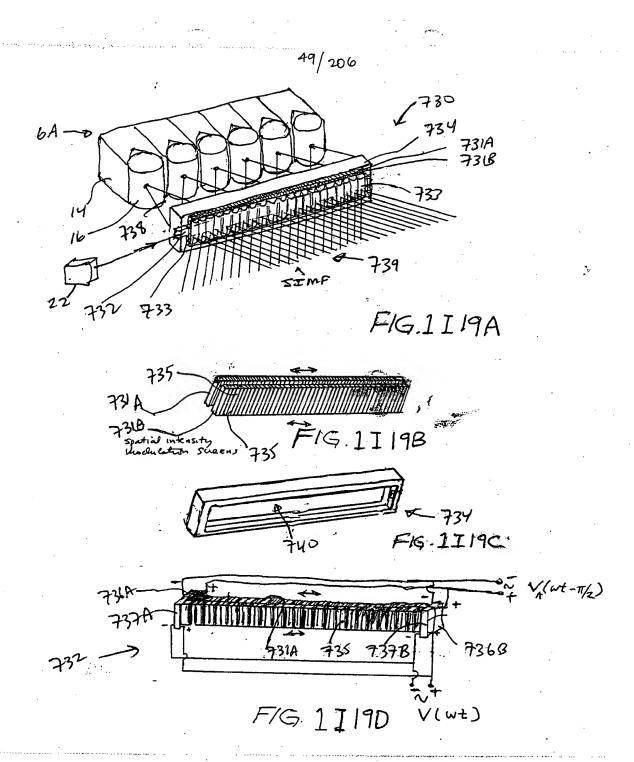


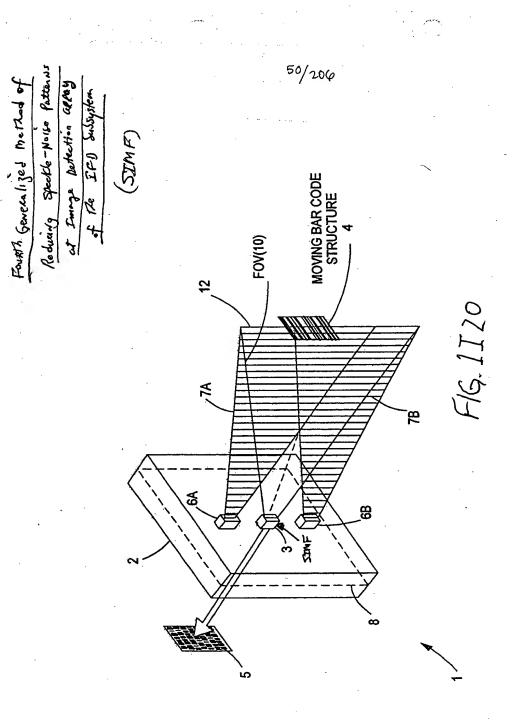
The Third Generalized Speckle-Noise Pattern Reduction Method Of The Present Invention

Prior to illumination of the target with the planar laser illumination beam (PLIB), modulate the spatial intensity of the transmitted PLIB along the planar extent thereof according to a spatial intensity modulation function (SIMF) so as to modulate the phase along the wavefront of the transmitted PLIB and produce numerous substantially different time-varying specklenoise patterns at the image detection array of the IFD Subsystem during the photo-integration time period thereof.

Temporally average the numerous substantially different time-varying speckle-noise patterns produced at the image detection array in the IFD Subsystem during the photo-integration time period thereof, so as to thereby reduce power of the speckle-noise pattern observed at the image detection array.

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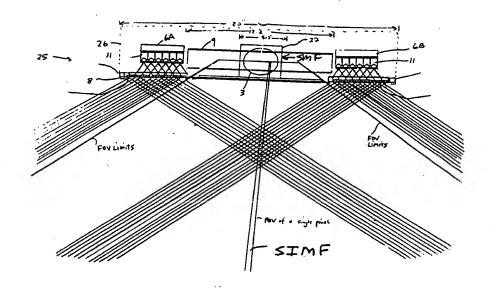


FIG.IIZIA

The FourthGeneralized Speckle-Noise Pattern Reduction Method Of The Present Invention

After illumination of the target with the planar laser illumination beam (PLIB), modulate the spatial intensity of the reflected/scattered (i.e. received) PLIB along the planar extent thereof according to a spatial intensity modulation function (SIMF) so as to modulate the phase along the wavefront of the received PLIB and produce numerous substantially different timevarying speckle-noise patterns at the image detection array of the IFD Subsystem during the photo-integration time period thereof.

Temporally average the many substantially different time-varying specklenoise patterns produced at the image detection array in the IFD Subsystem during the photo-integration time period thereof, so as to thereby reduce the speckle-noise pattern observed at the image detection array.

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FIG. 1IZ1B



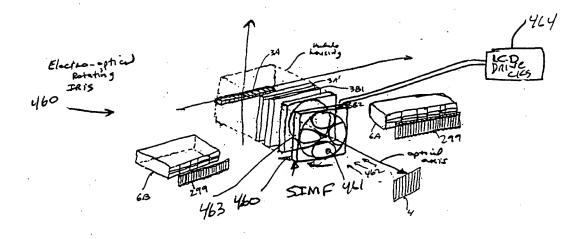


FIG.1IZZA

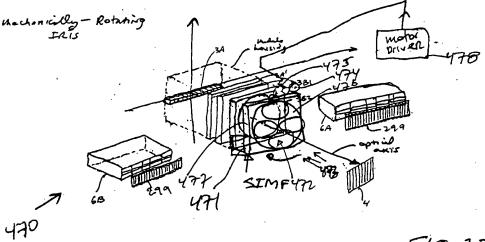
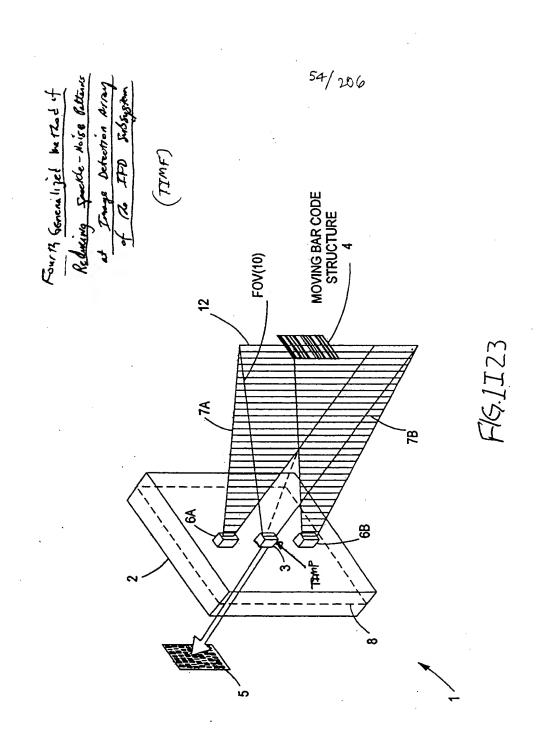


FIG. 1IZZB



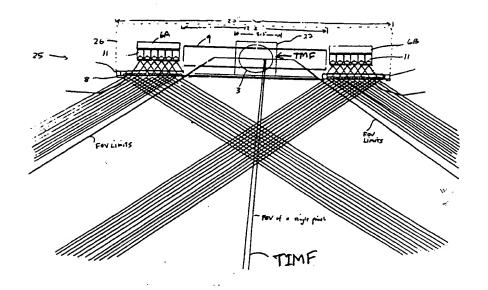


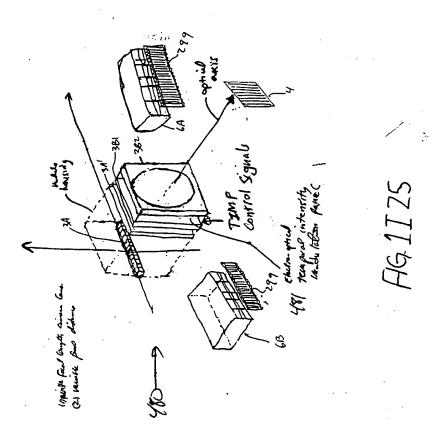
FIG.1I24A

The Fifth Generalized Speckle-Noise Pattern Reduction Method Of The Present Invention

After illumination of the target with the planar laser illumination beam (PLIB), modulate the temporal intensity of the reflected/scattered (i.e. received) PLIB along the planar extent thereof according to a temporal intensity modulation function (TIMF) so as to modulate the phase along the wavefront of the received PLIB and produce many substantially different time-varying speckle-noise patterns at the image detection array of the IFD Subsystem during the photo-integration time period thereof.

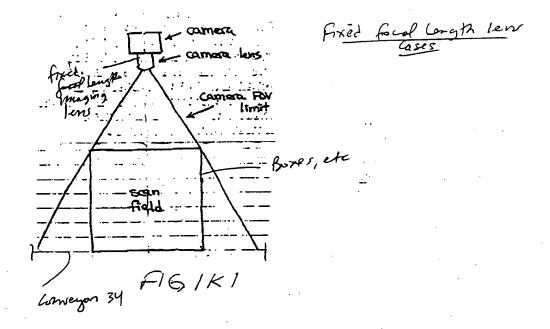
Temporally average the many substantially different time-varying specklenoise patterns produced at the image detection array in the IFD Subsystem during the photo-integration time period thereof, so as to thereby reduce the speckle-noise pattern observed at the image detection array.

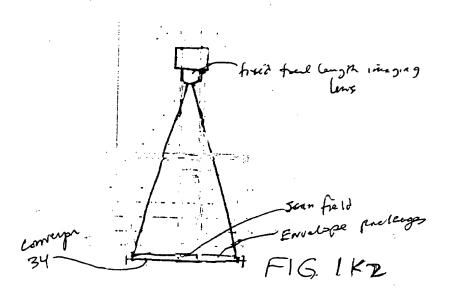
FIG.1I24B

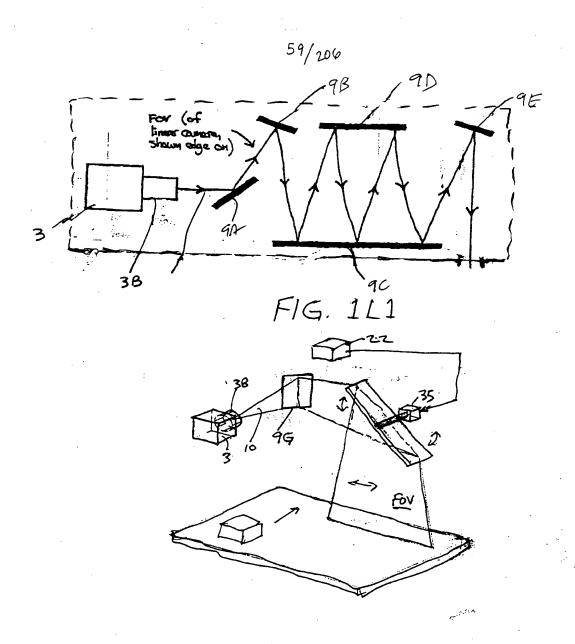


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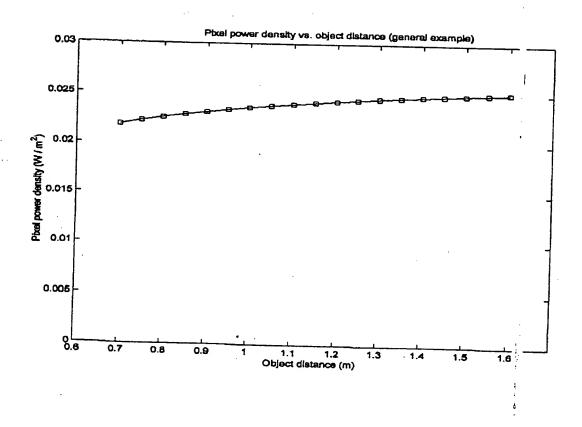
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F16.1L2



F19-1M1

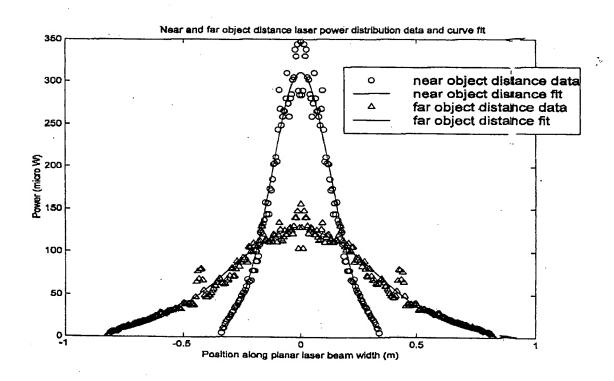
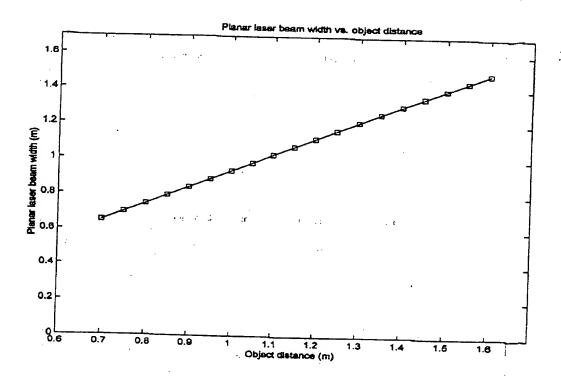
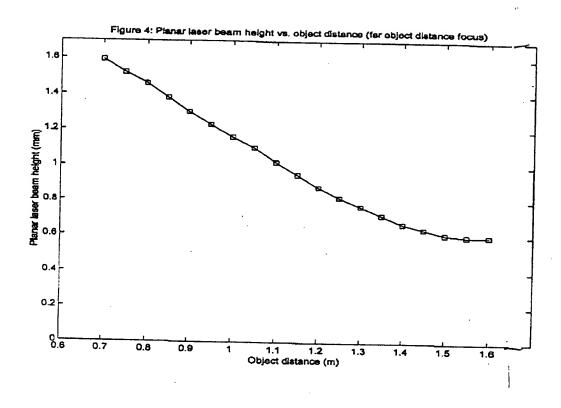


FIG./MZ



F16.1M3



F16-1M4

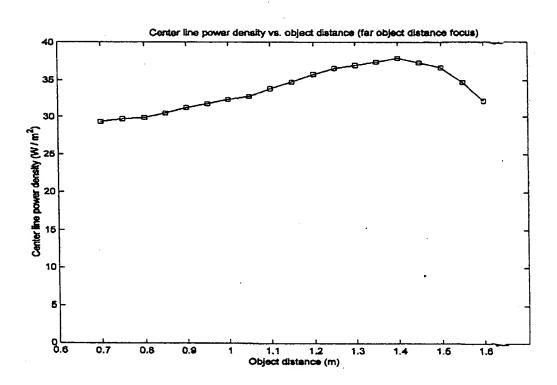
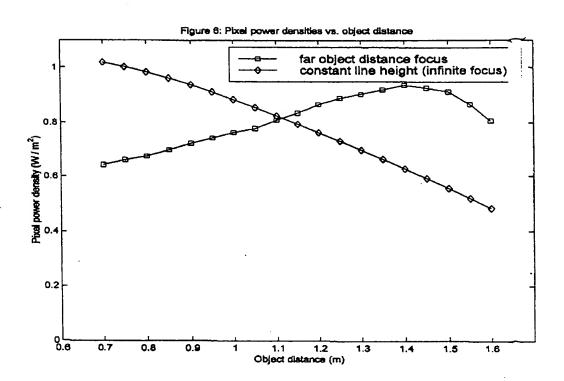


FIG. IN



F1G.10

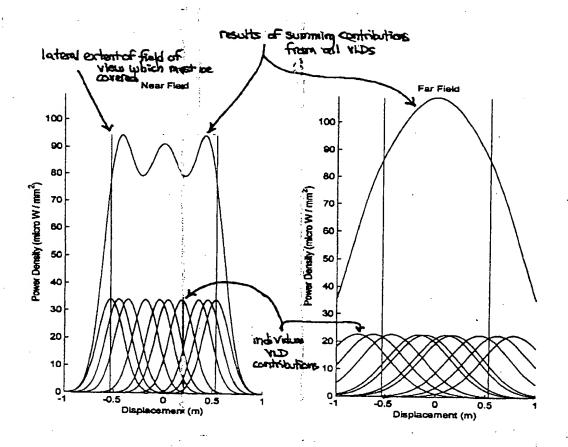
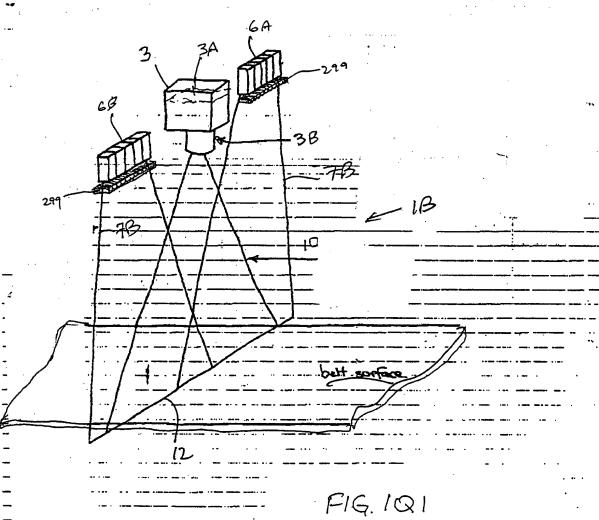
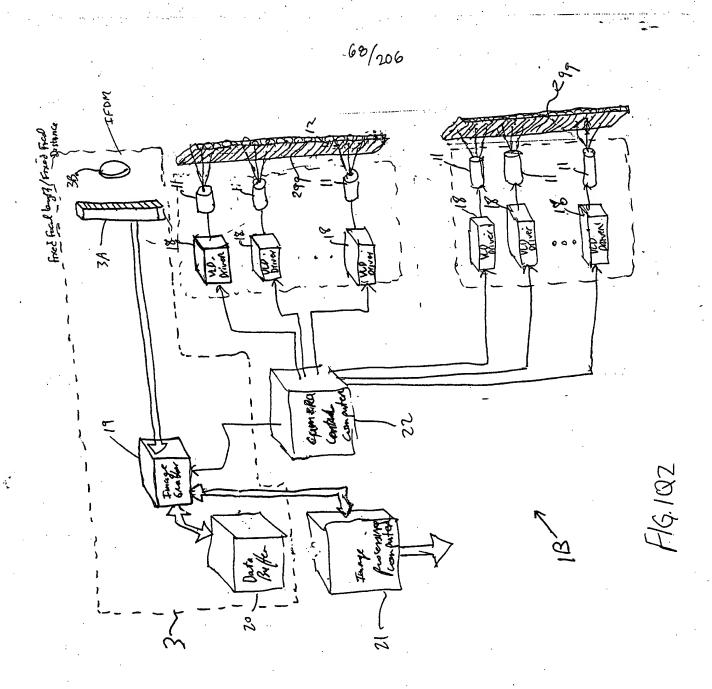


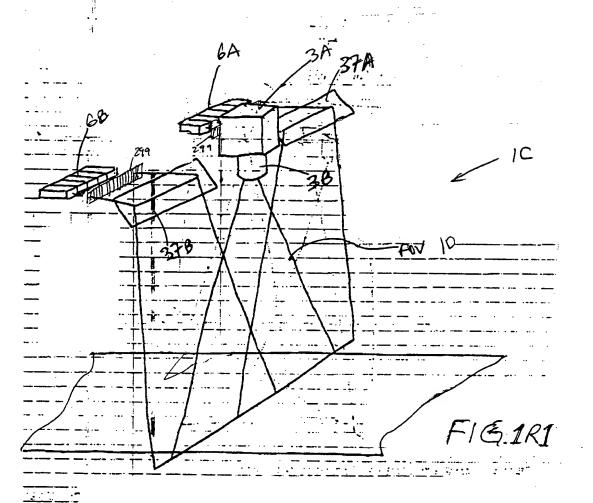
FIG.1P1

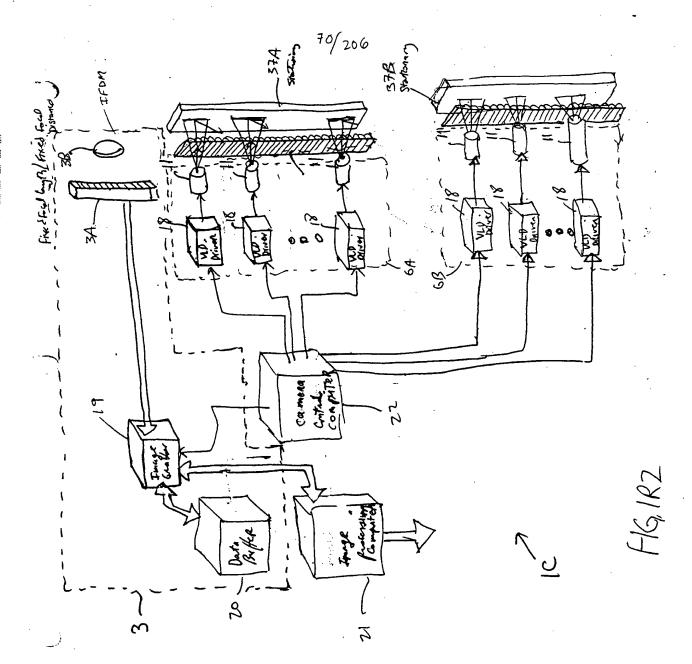
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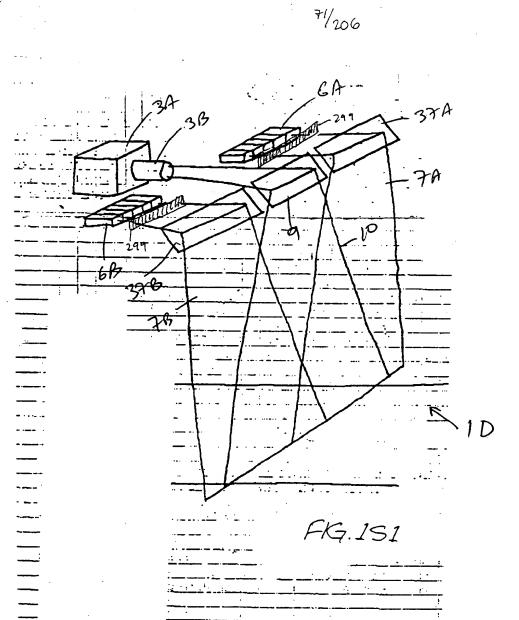








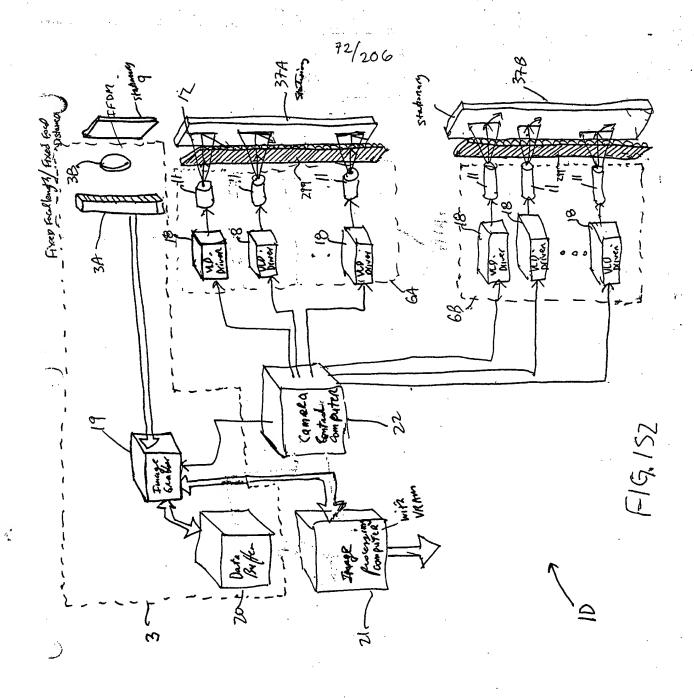




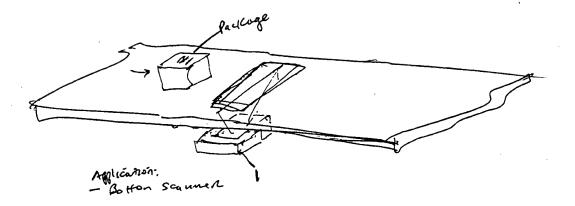
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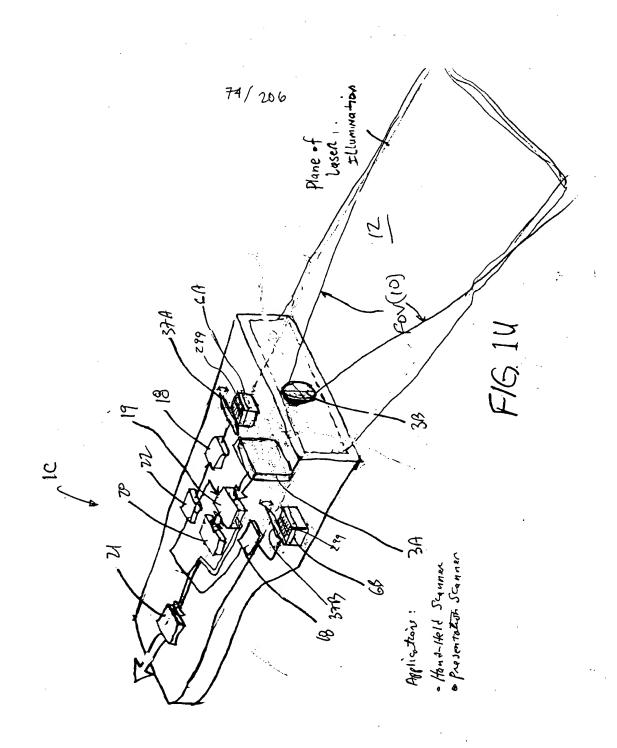
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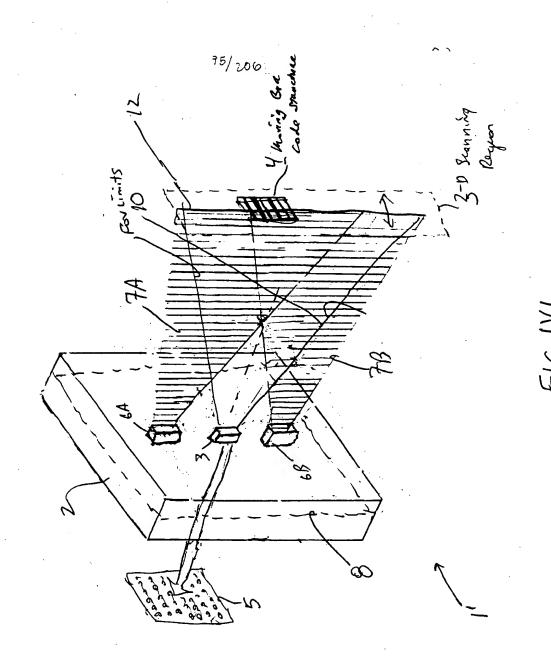


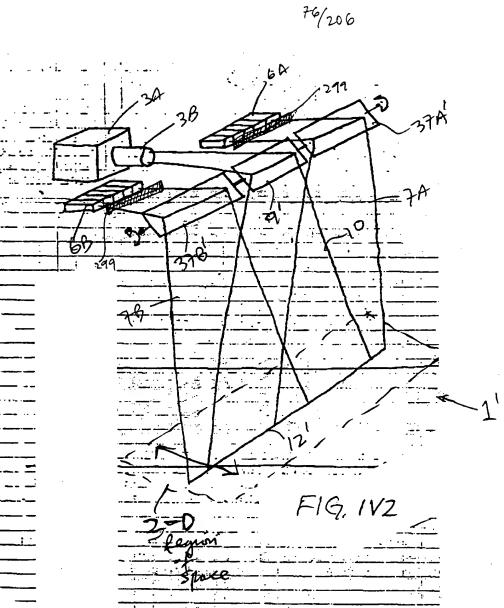
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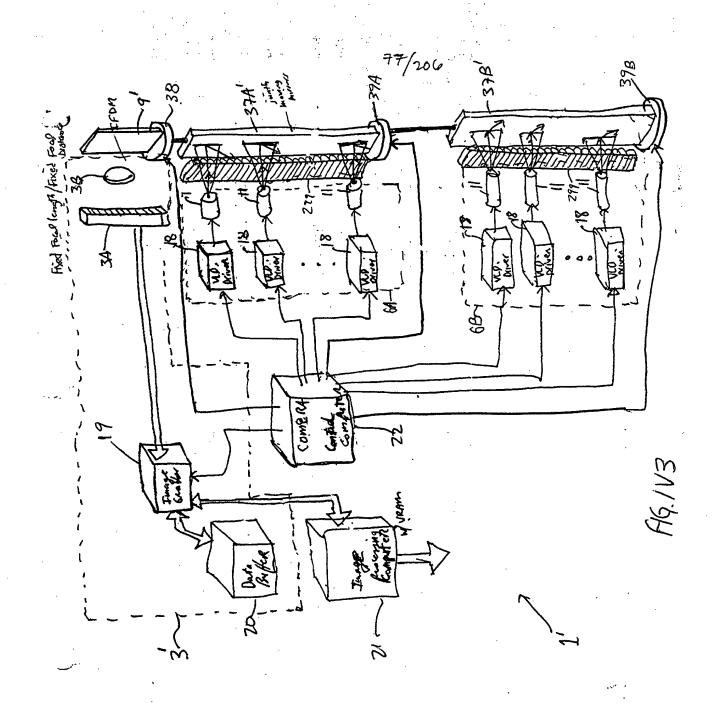


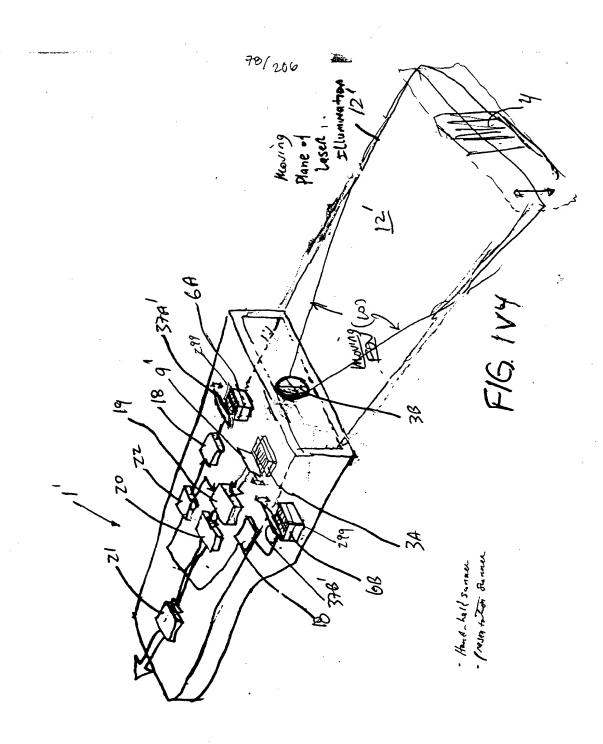
HG IT



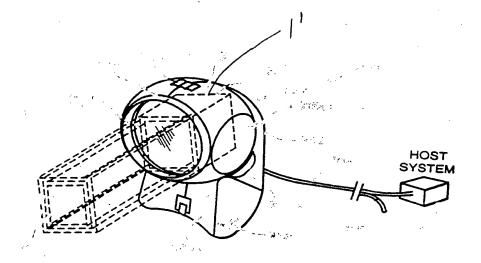




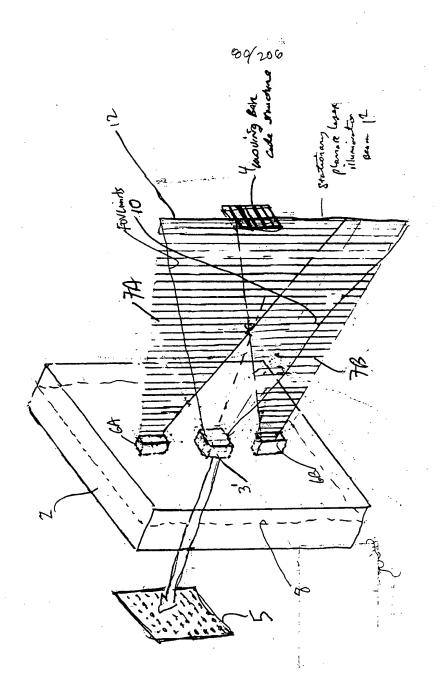




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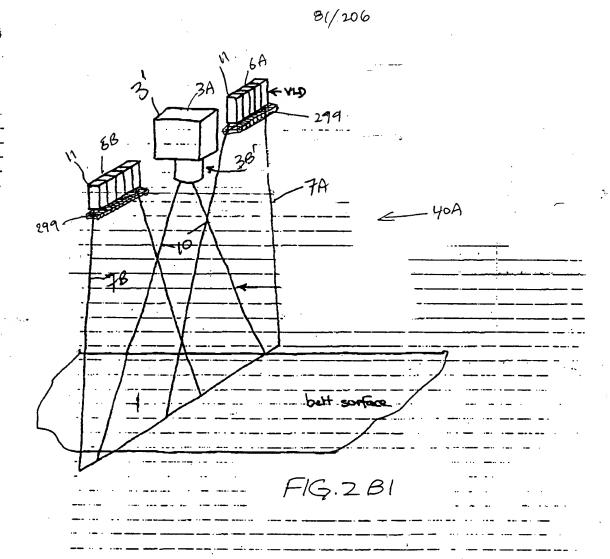


(Presentation type summer)
FIG. 1 V5

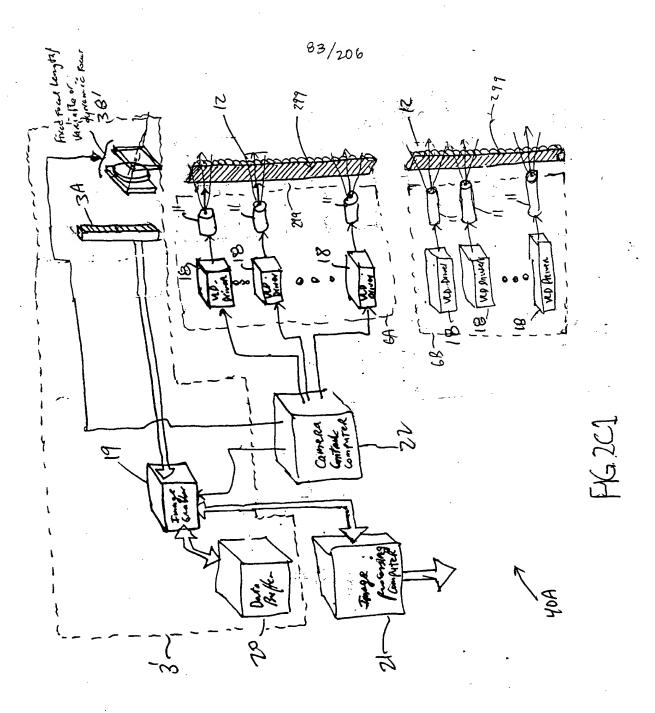


F1G. 2A

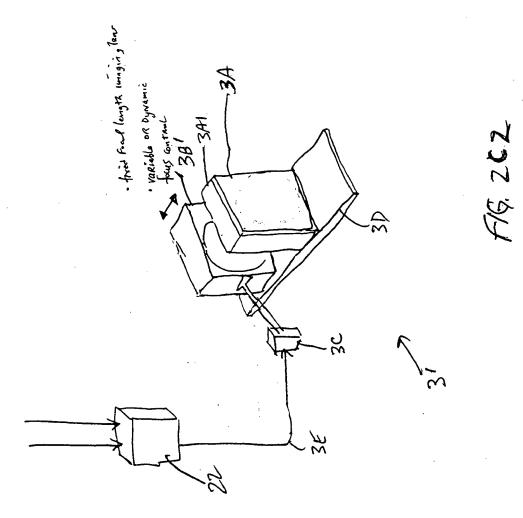
, ₂



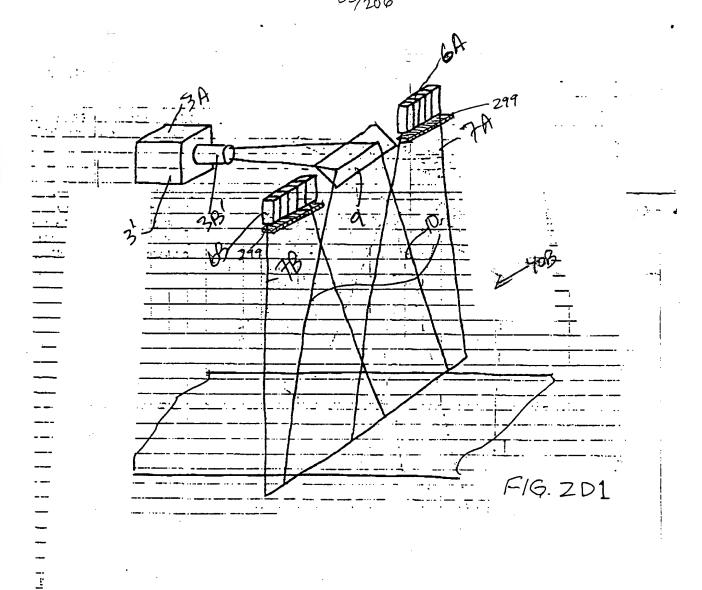
F1G 282

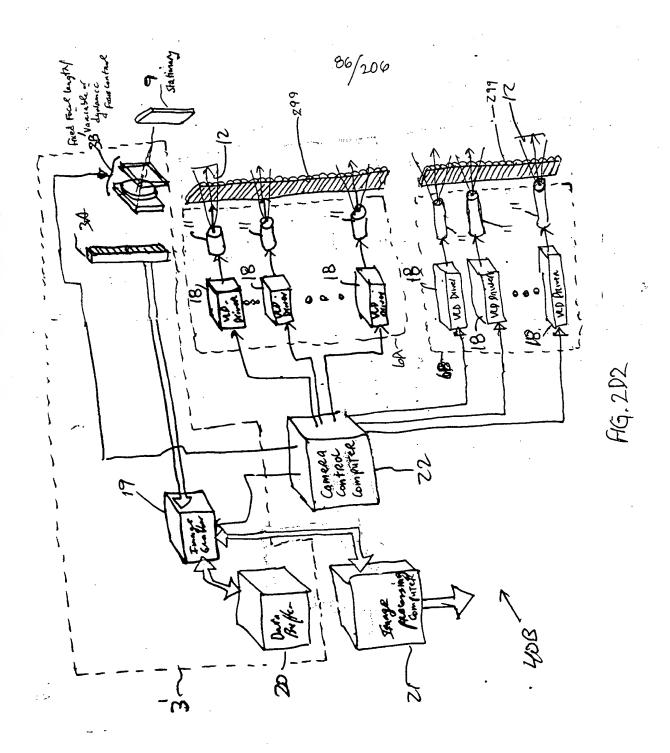


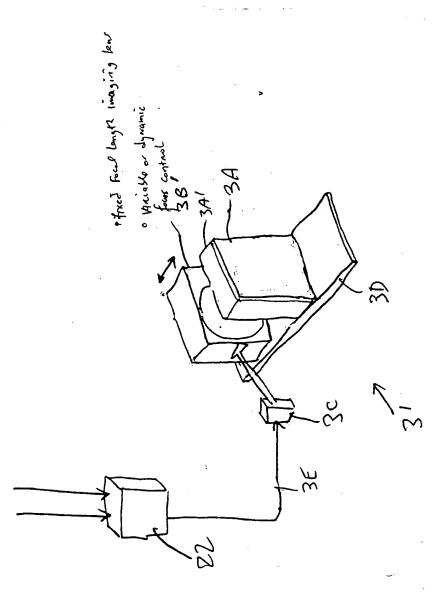
 \bigcirc



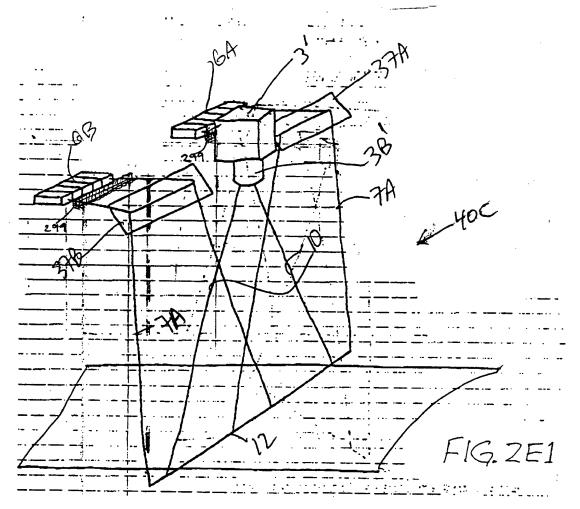
84/206







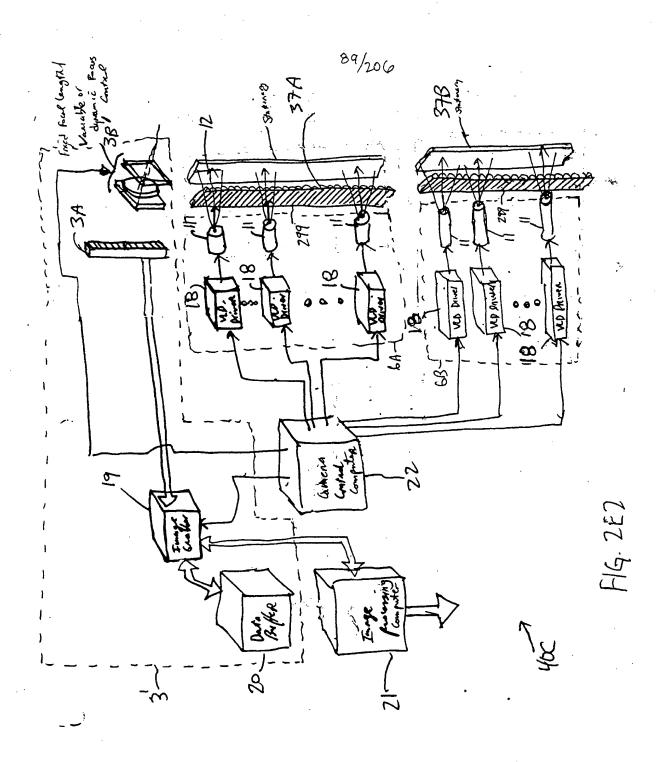


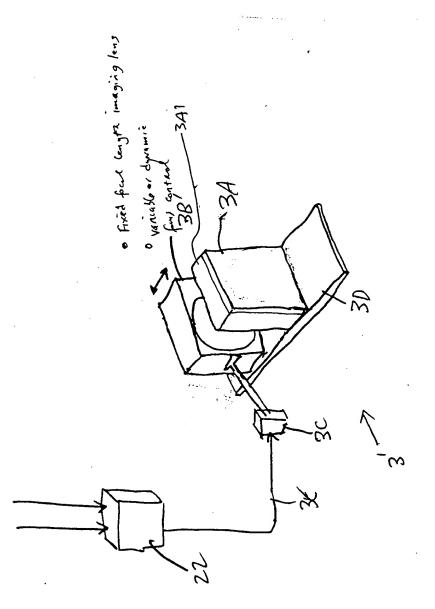


- - -

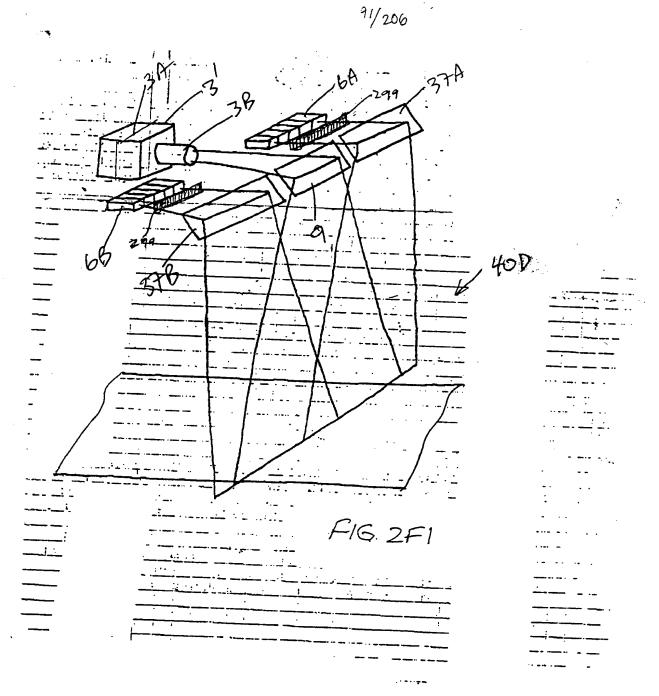
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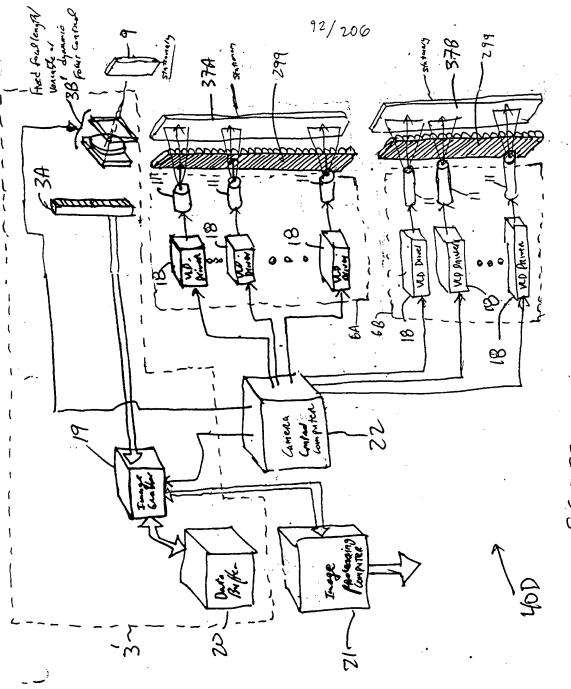
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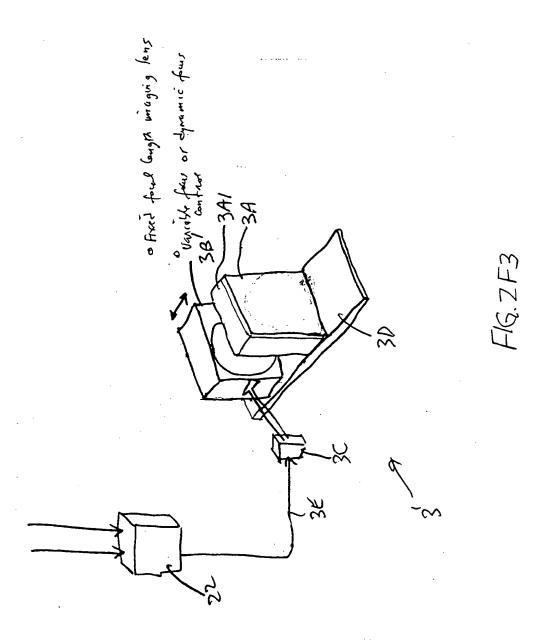


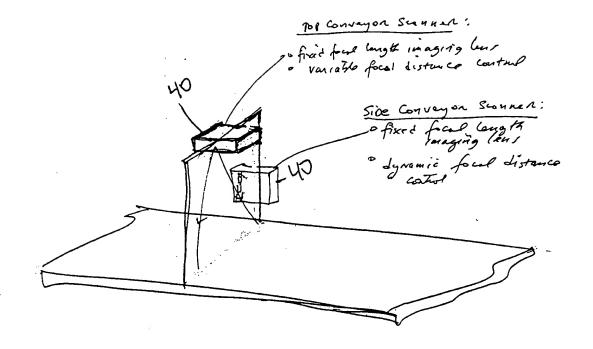
F/G. 2.83



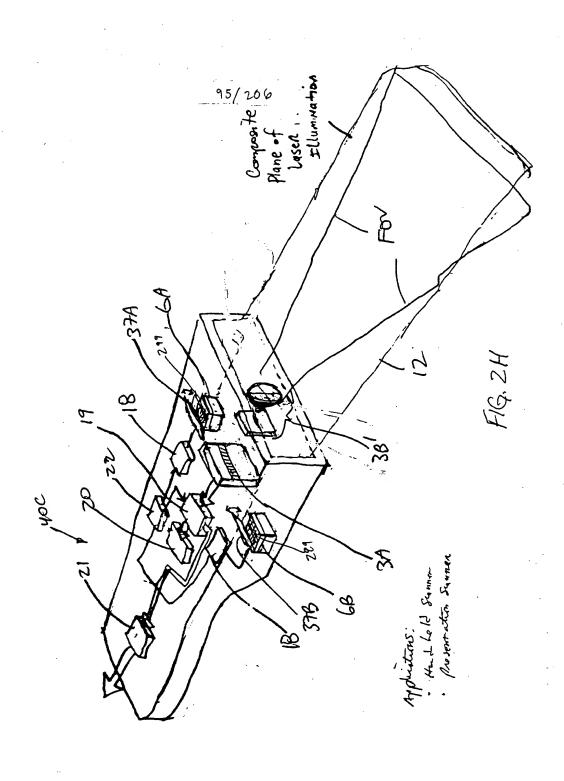


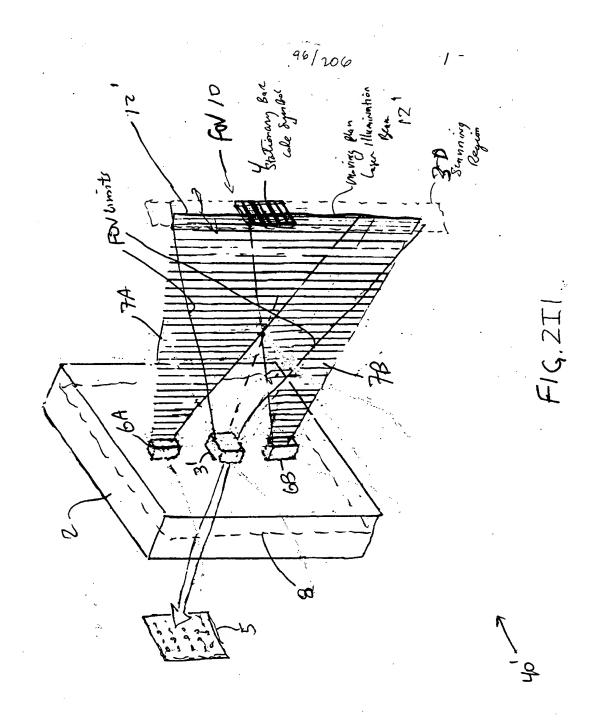
F1G, 2F2

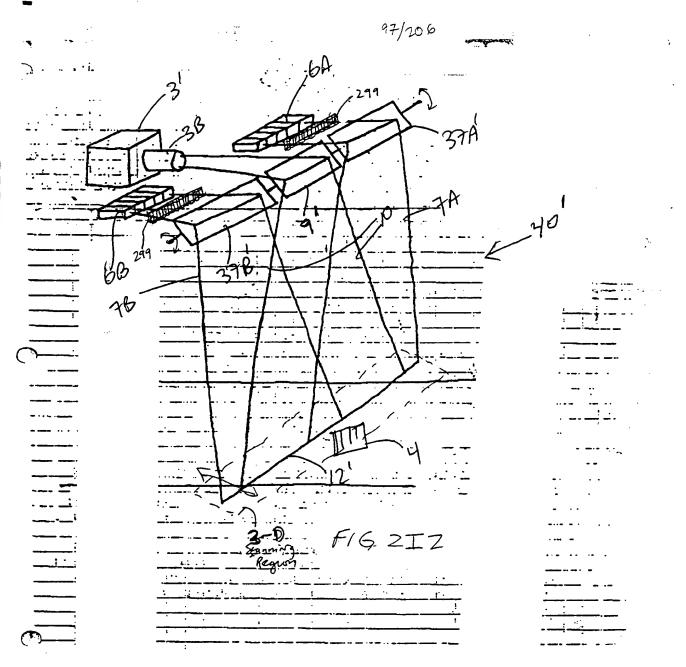


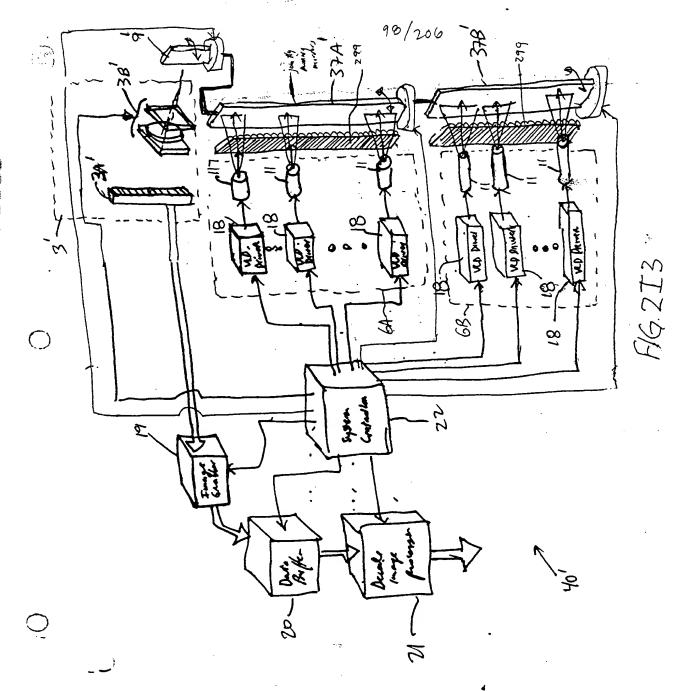


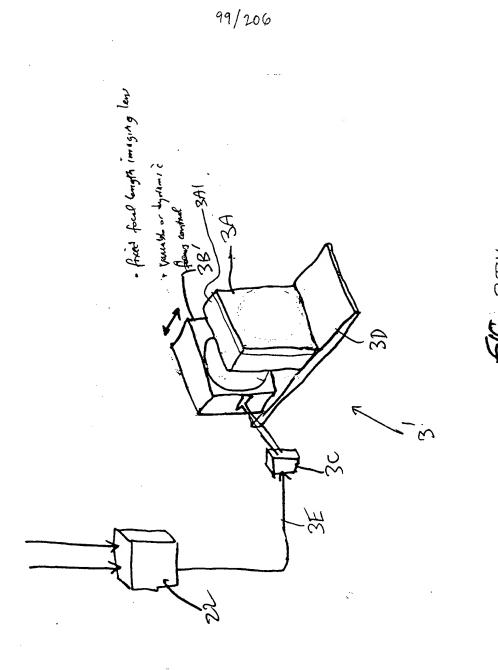
F1G. 2G

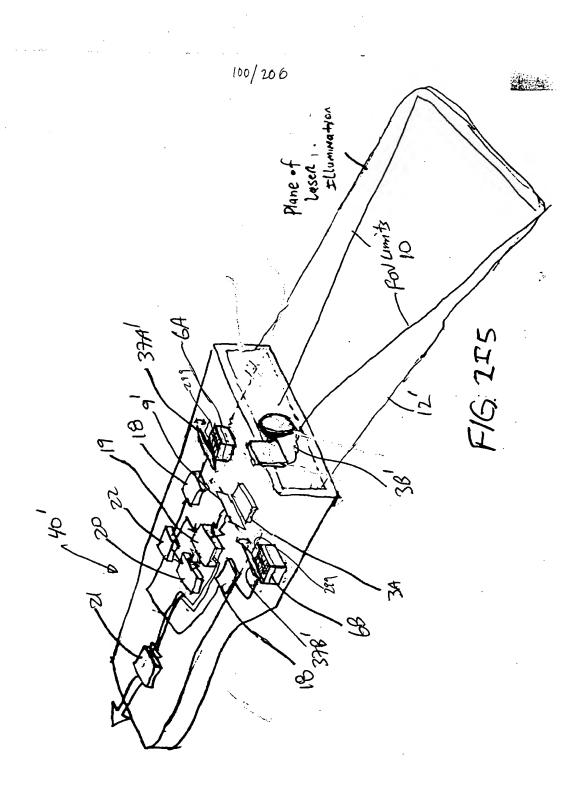


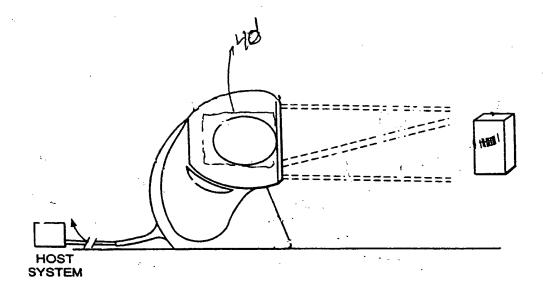




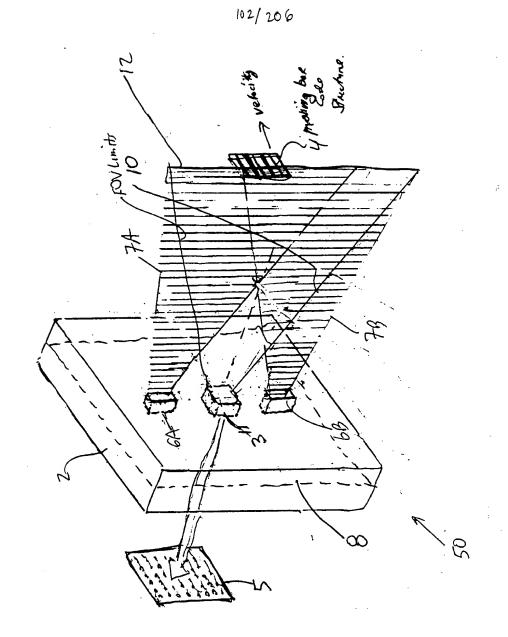


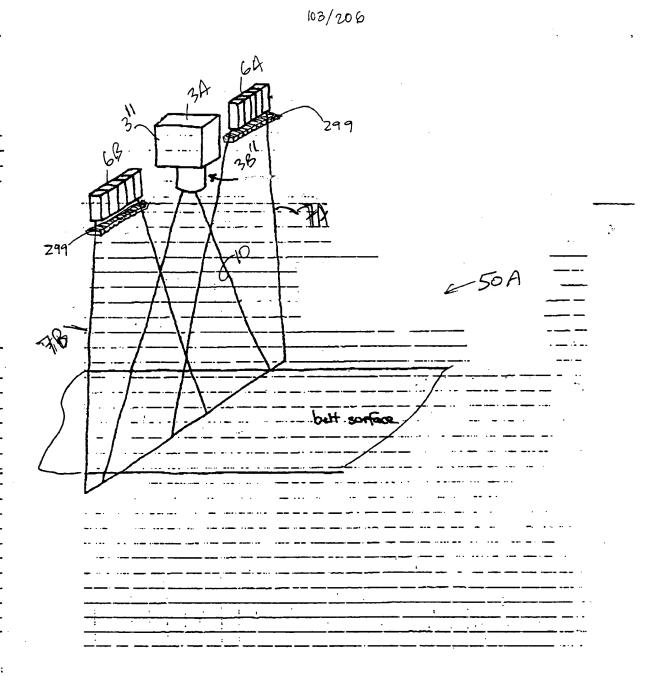






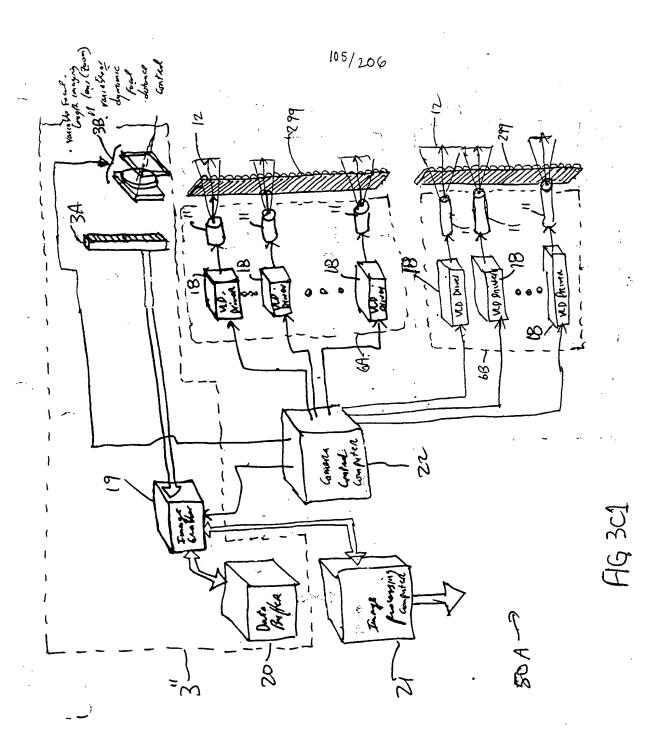
F1G. 2I6

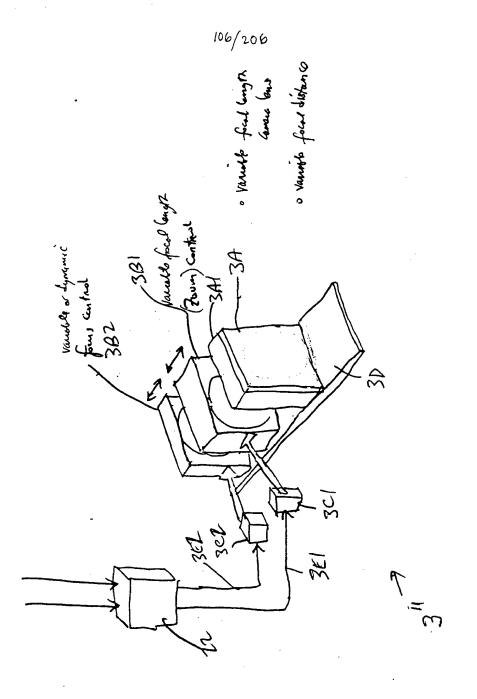




F16,3B1

r16,382





F16, 3CZ

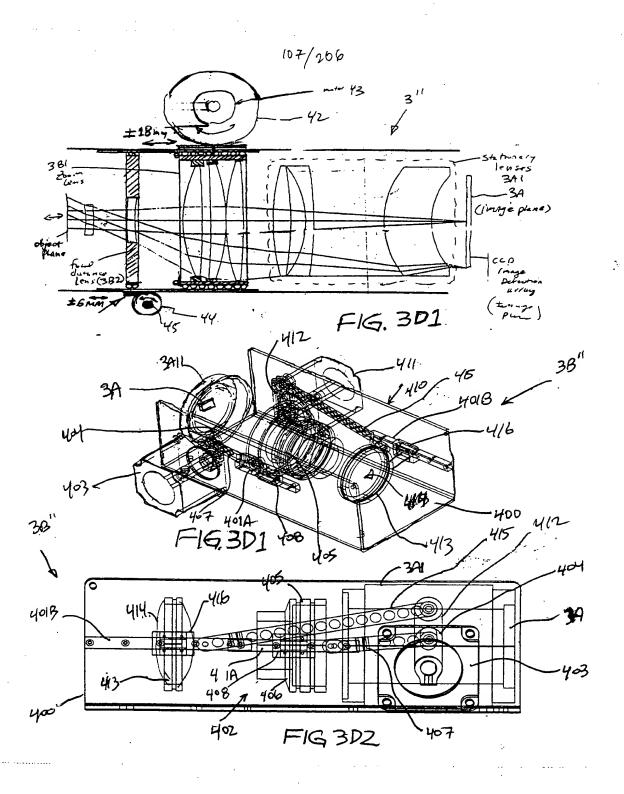
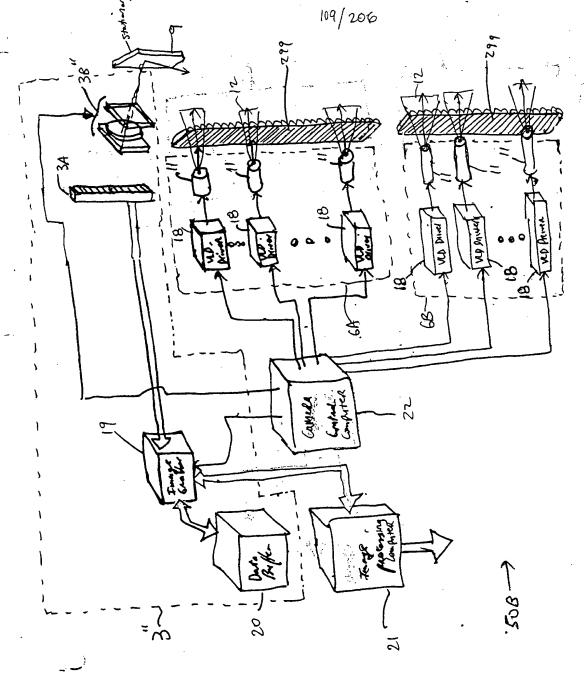
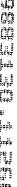
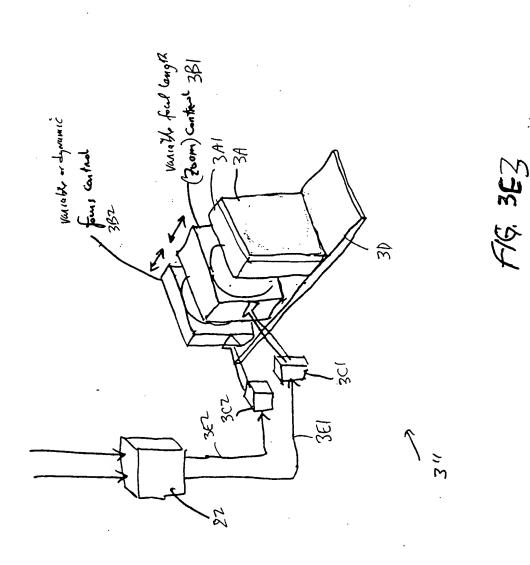


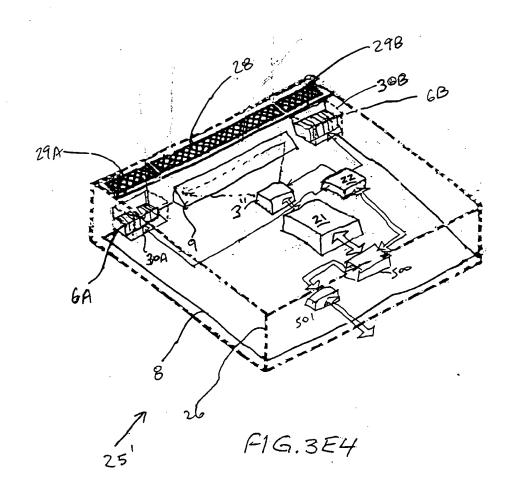
FIG 3EI



AG.3E2

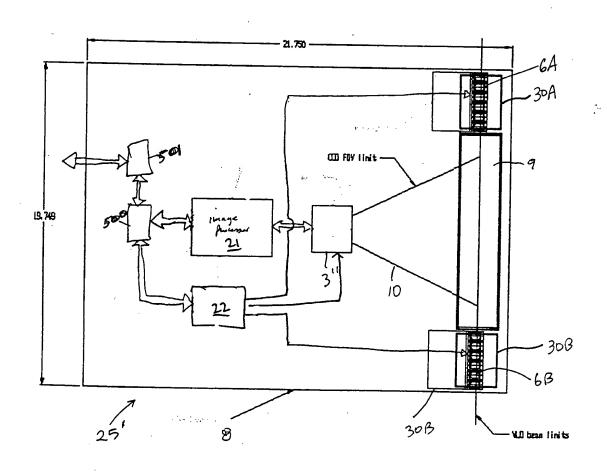






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F16. 3E5

F16 3E6

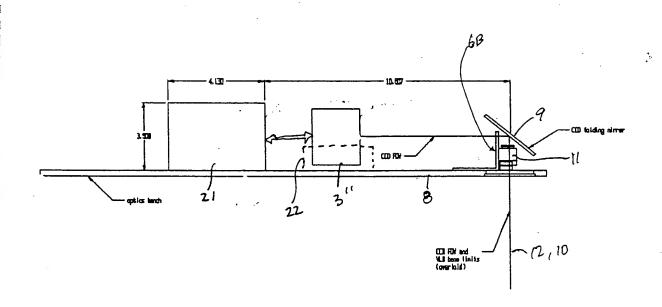
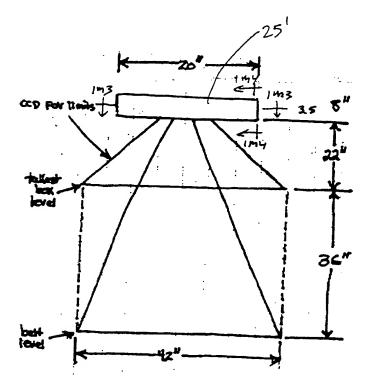


FIG. BE7

* variable FOY



F16.3E8

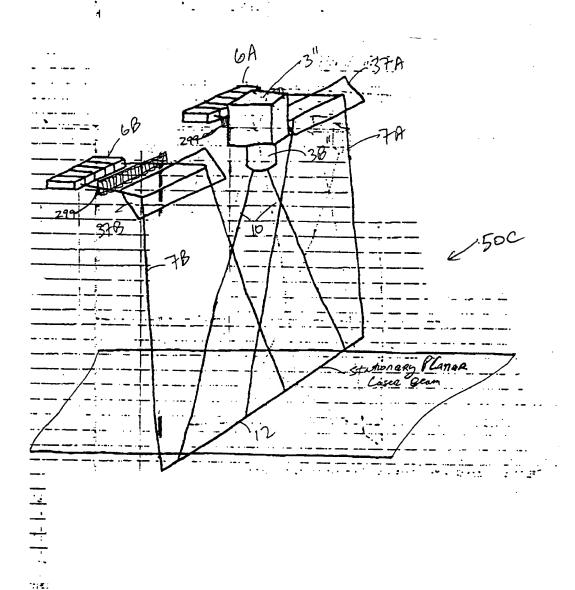
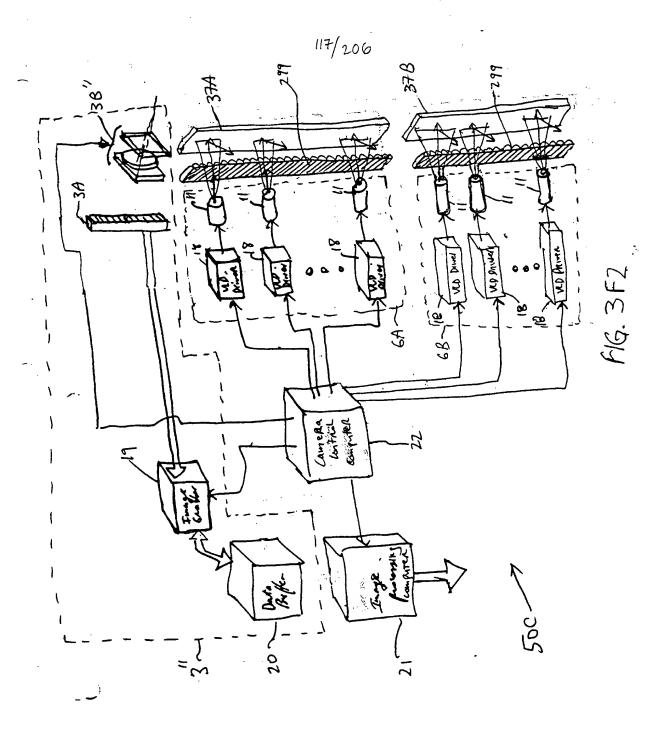
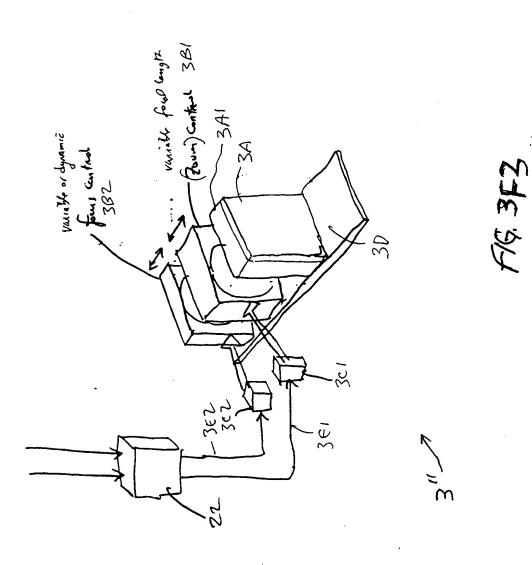
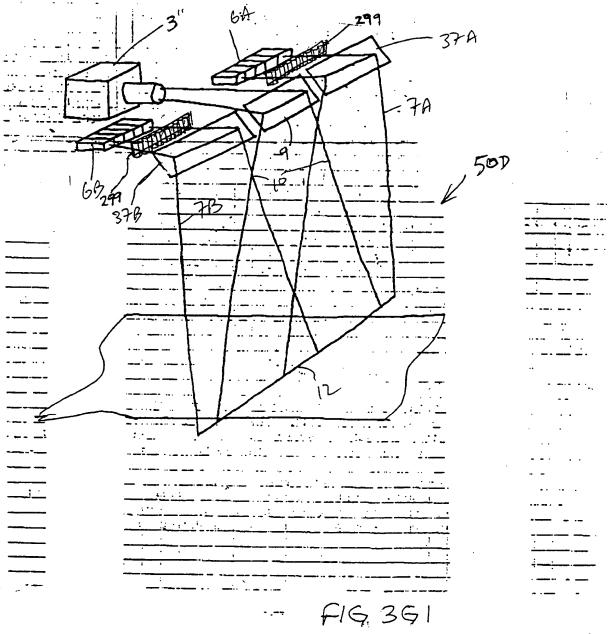
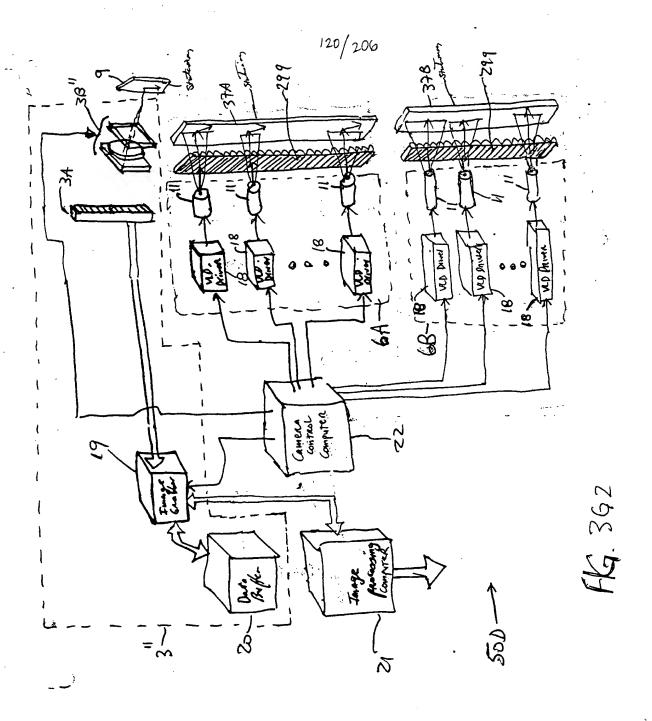


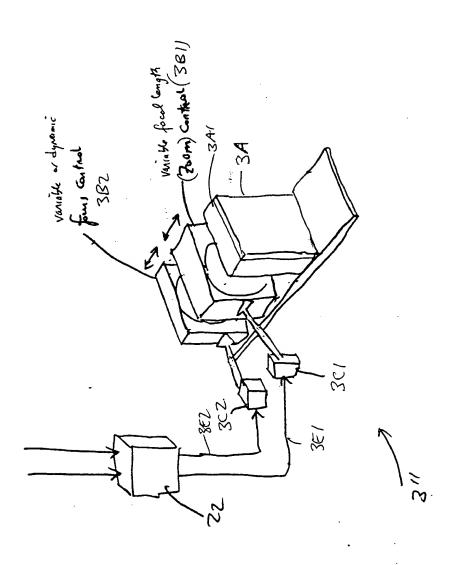
FIG. 3F1











F/G. 393

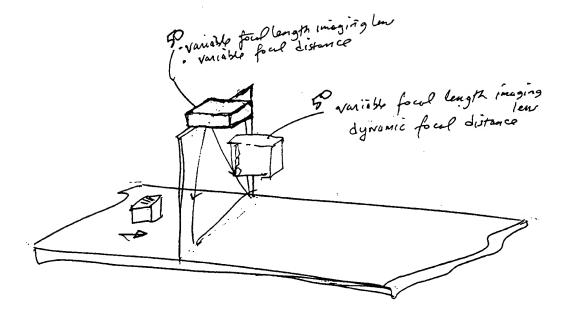
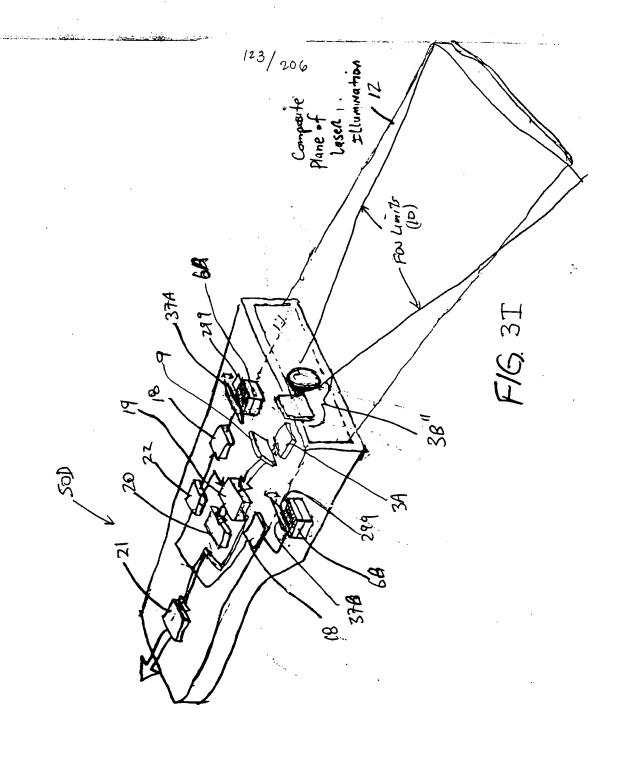
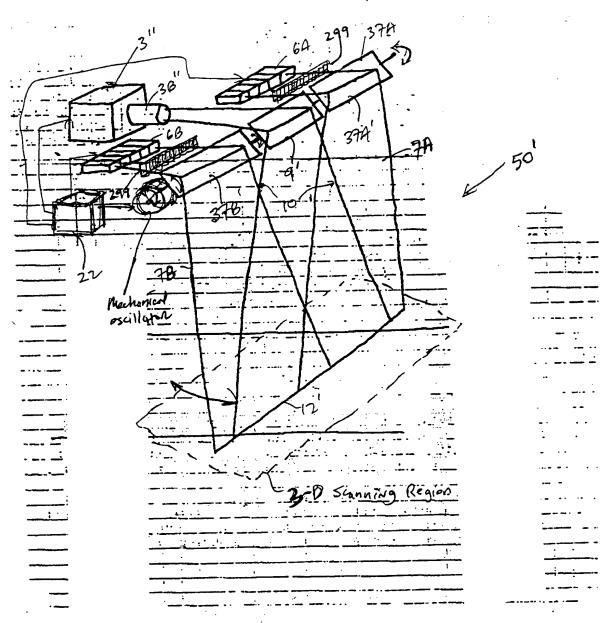


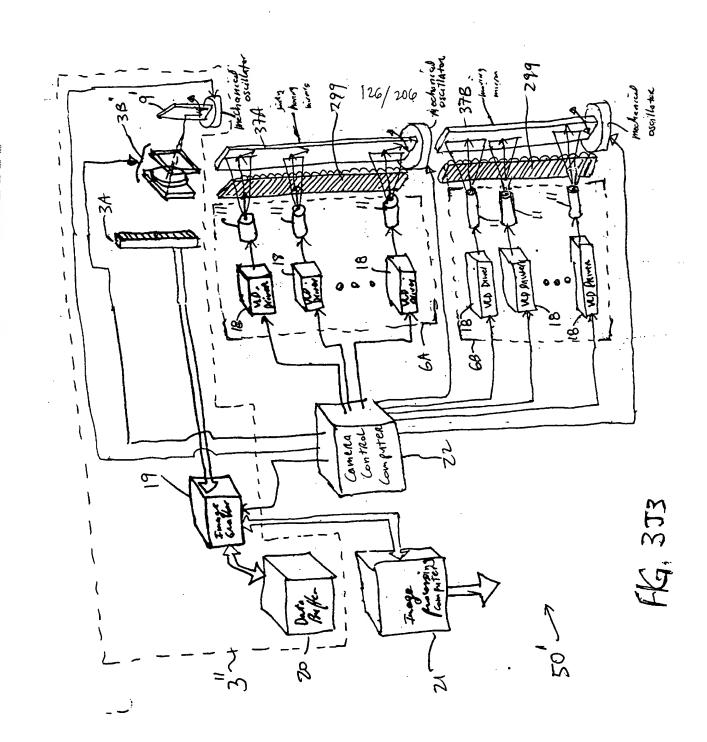
FIG. 3H



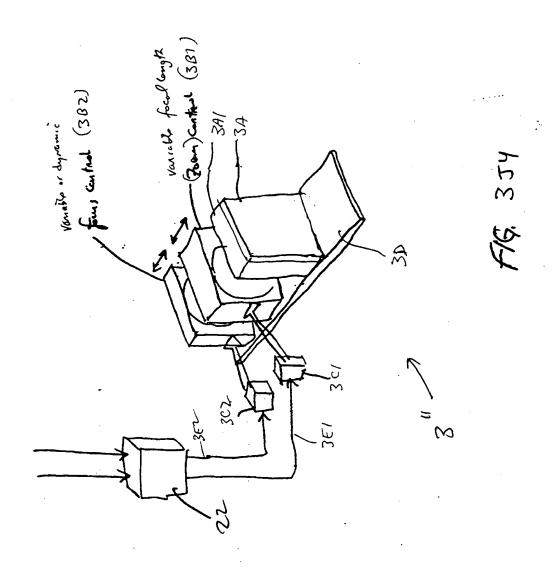
F1G, 311

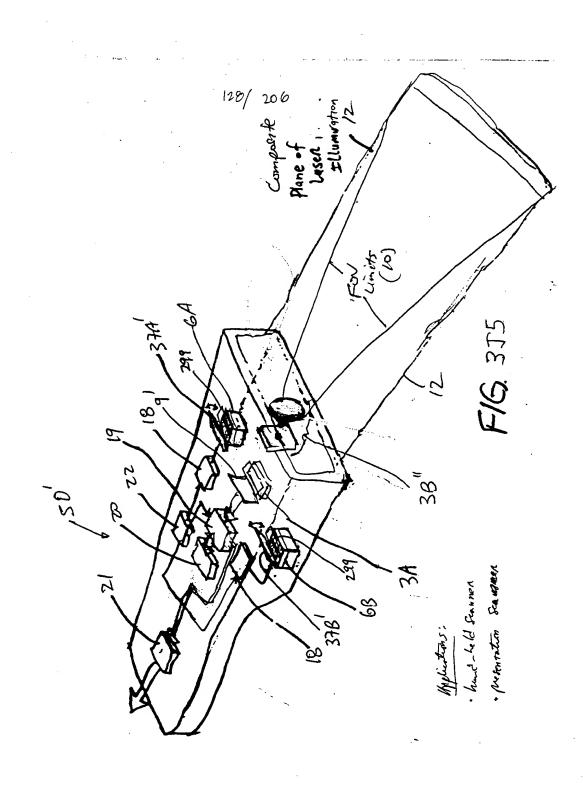


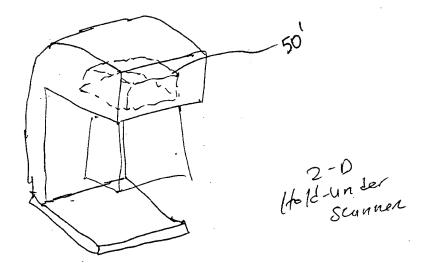
F1G, 3JZ



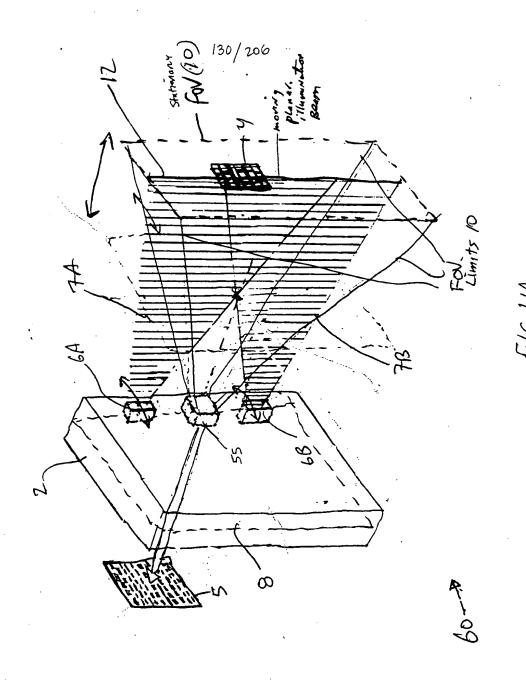


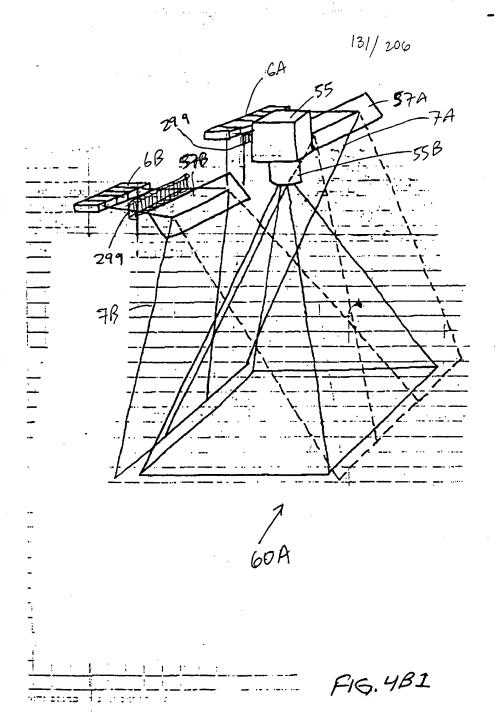


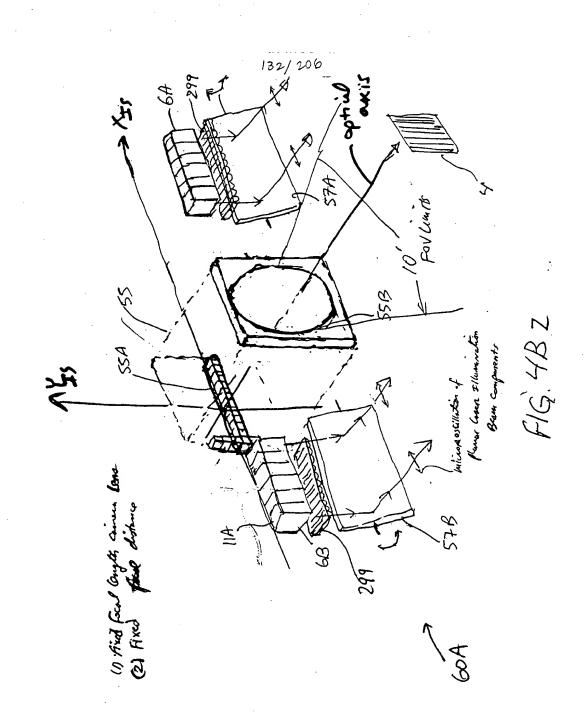


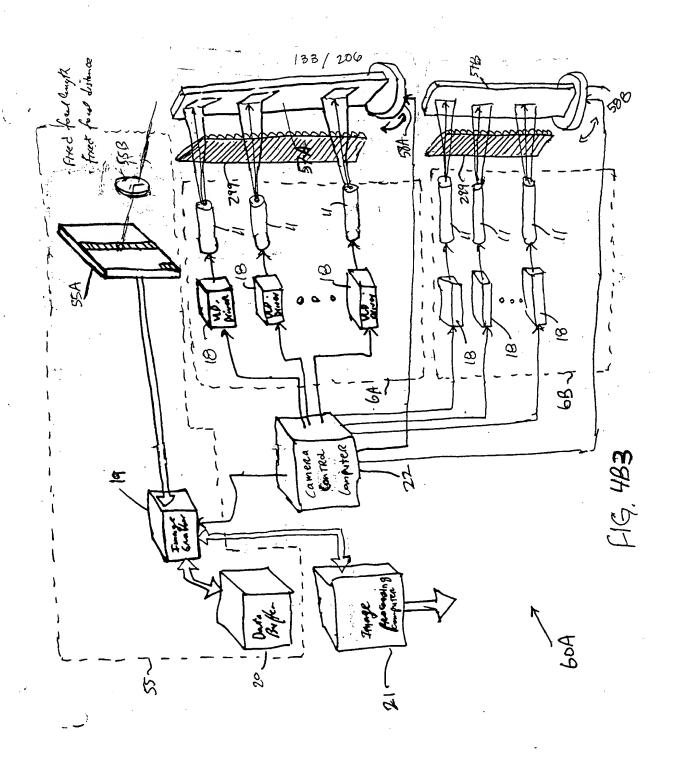


F1G-3J6

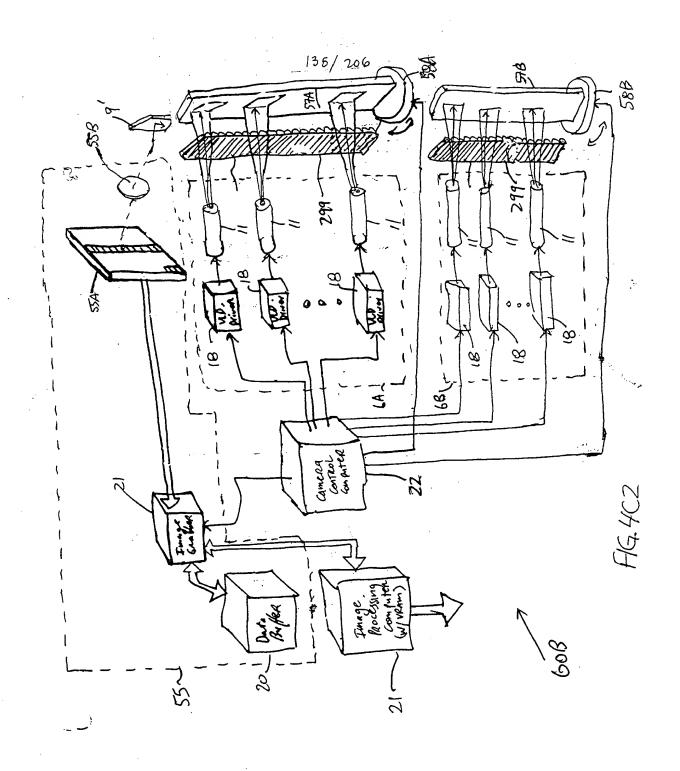








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299 7B	55 55B 10' CA 299 37A methon os	((10') Limits
Machanical ascillaton (58B)	608	



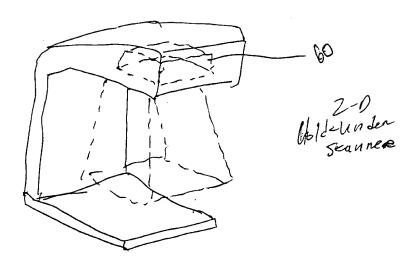
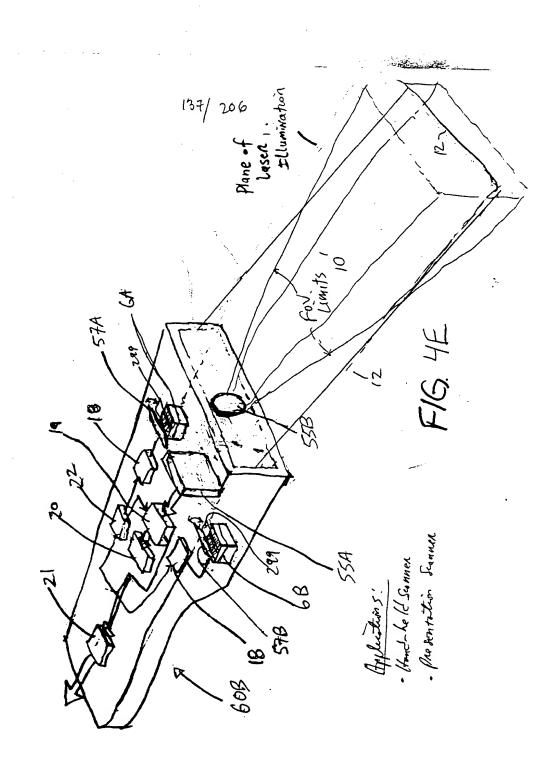
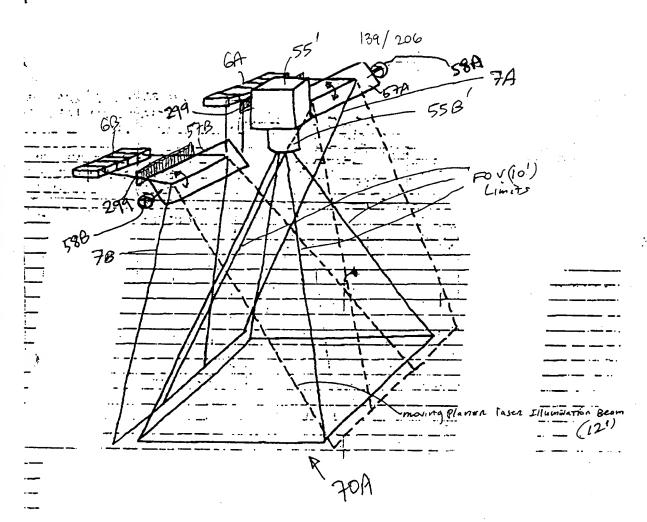


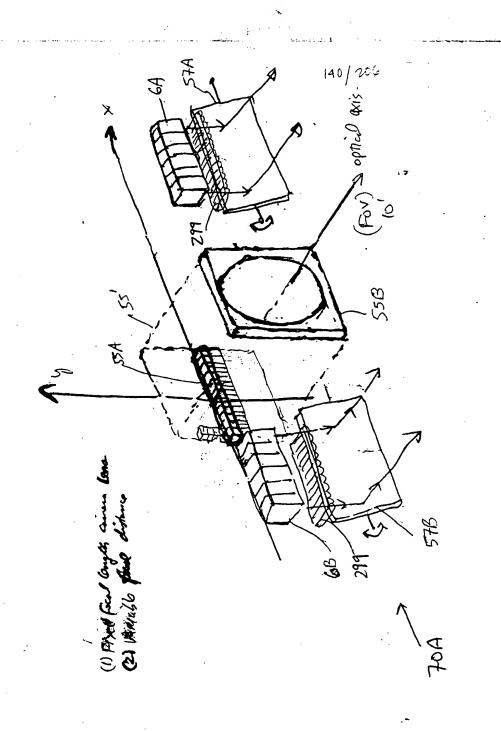
FIG.4D



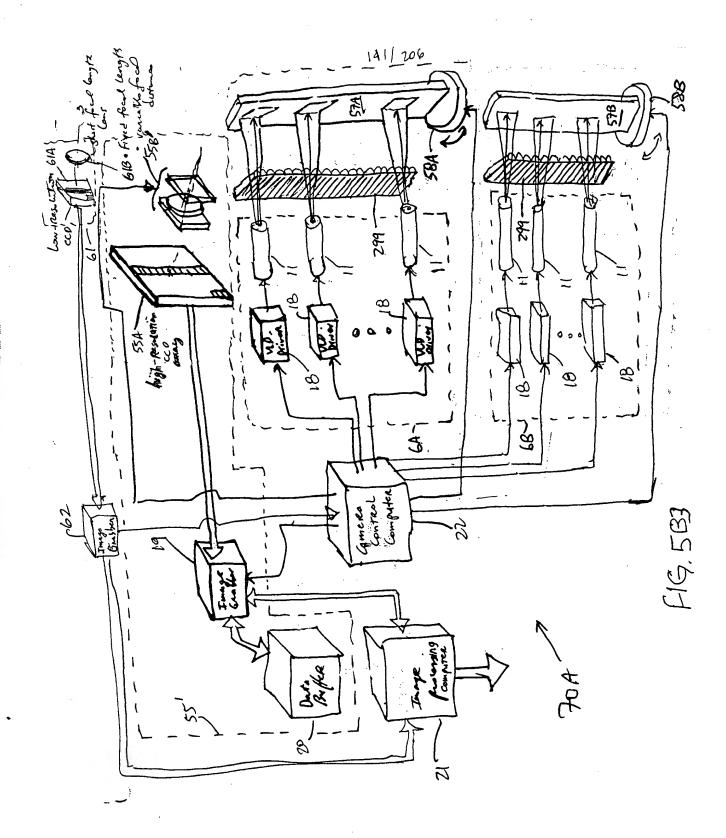
(3)



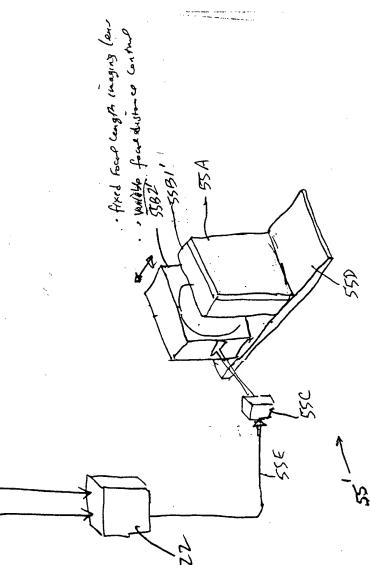
F16.581

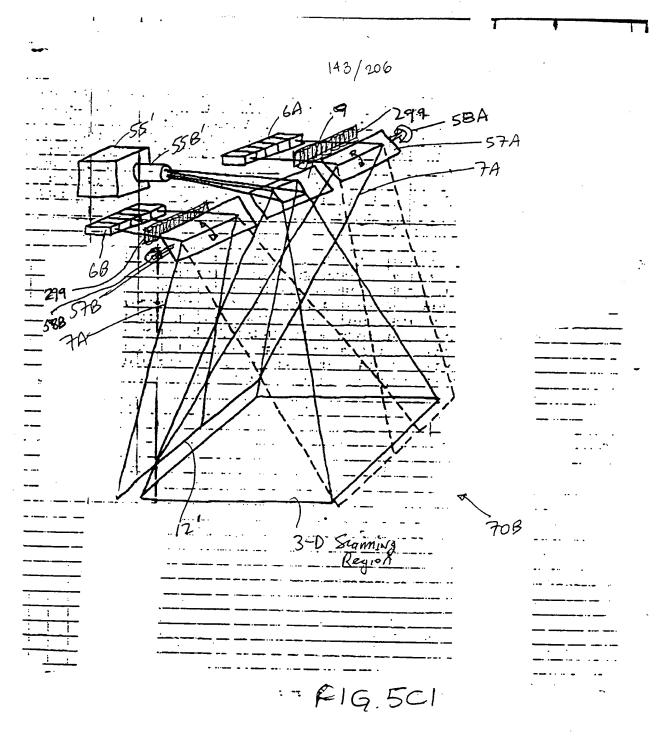


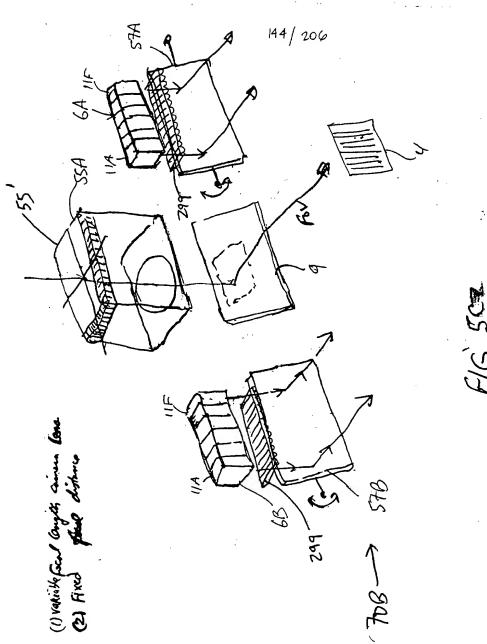
F1G, 581

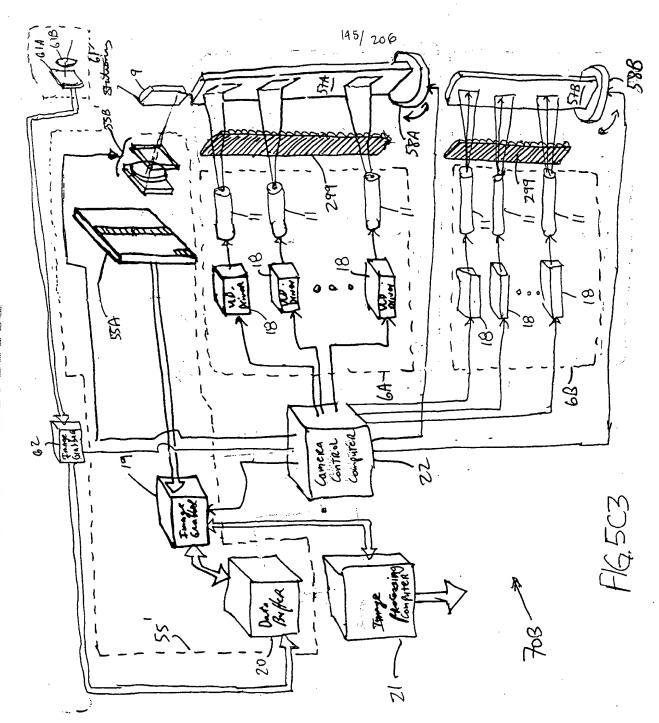




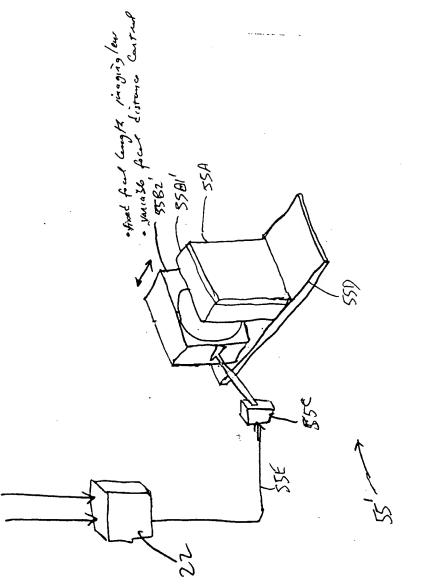




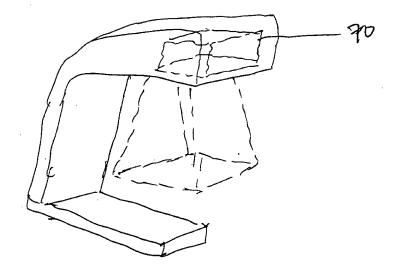








F1G. 5C4



F1G. 5D

F19.6A

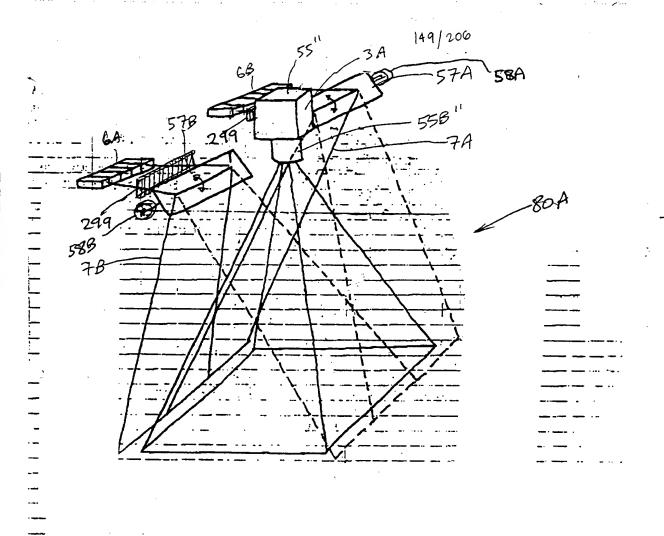
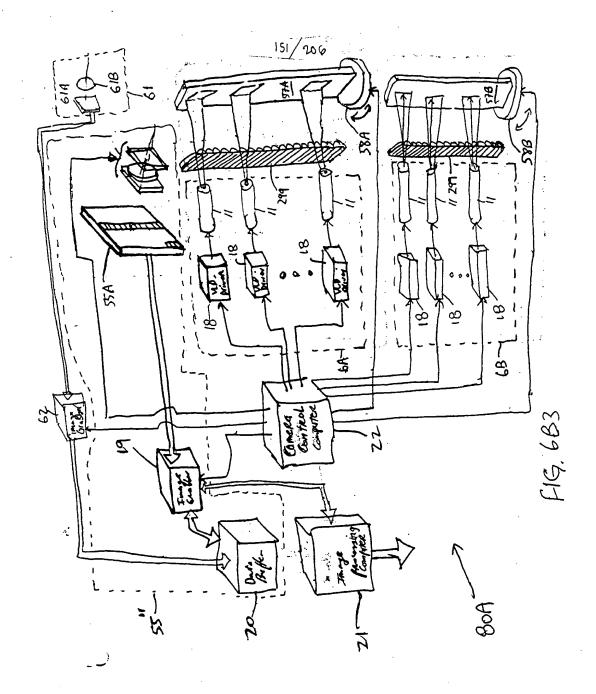
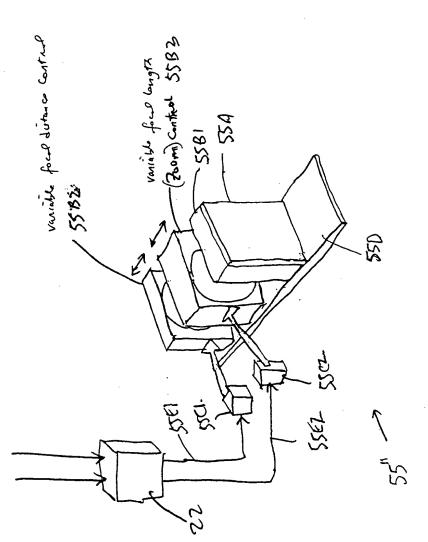
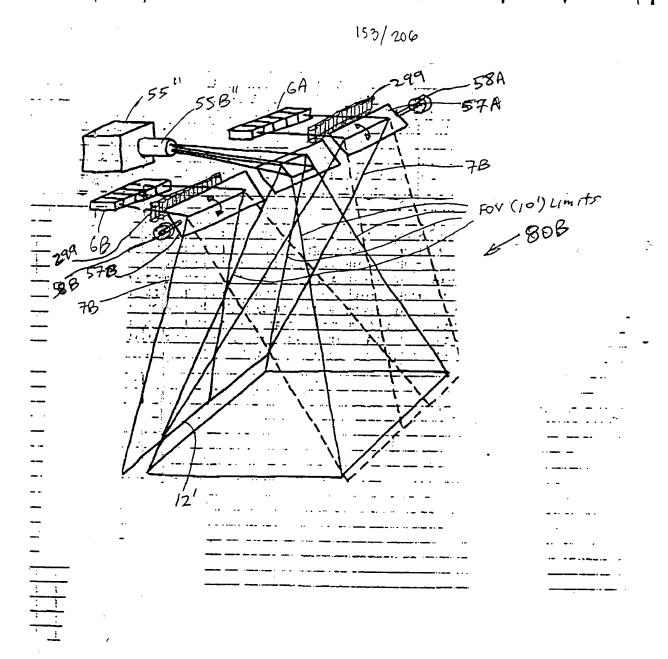


FIG. 681

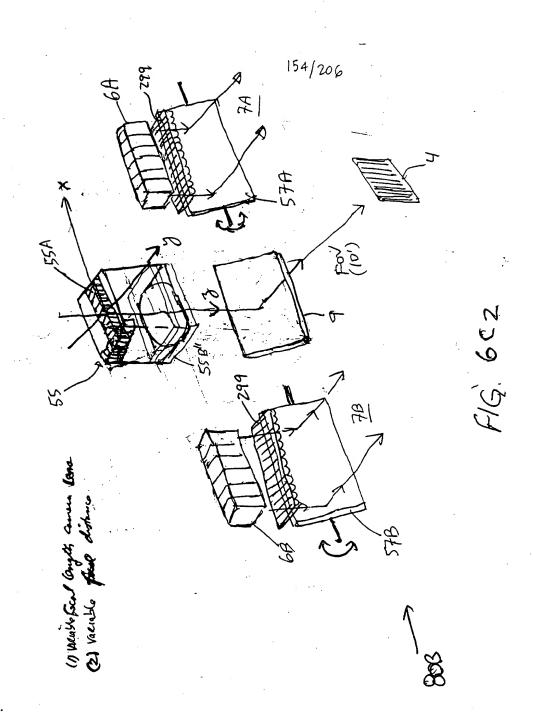


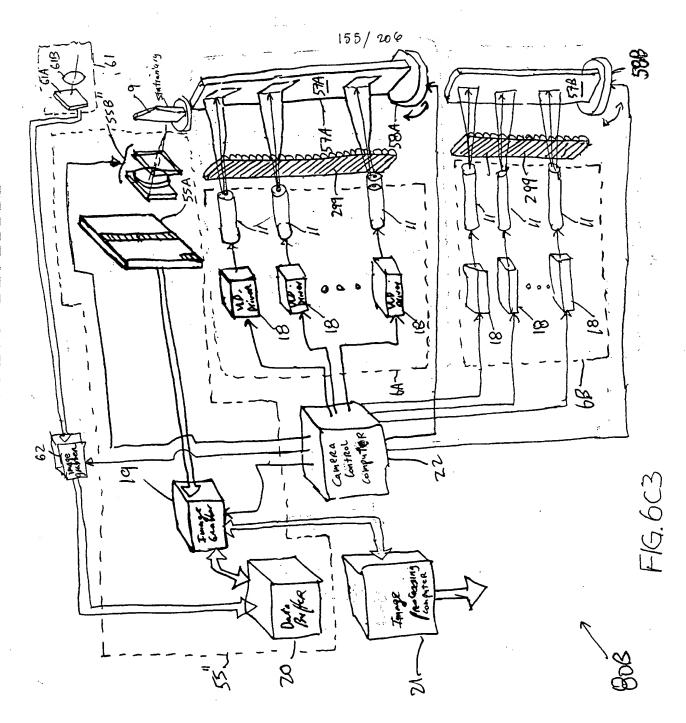


F1G. 684

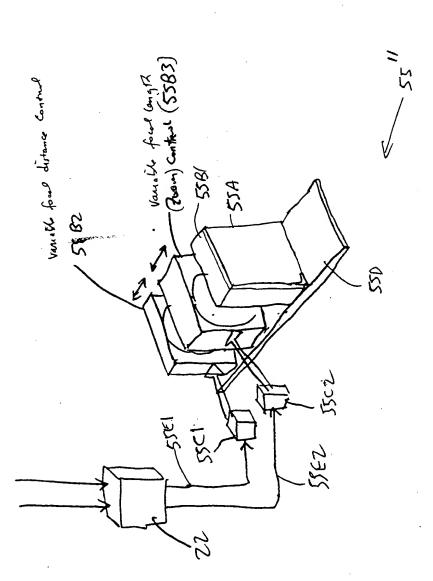


F19.6C1



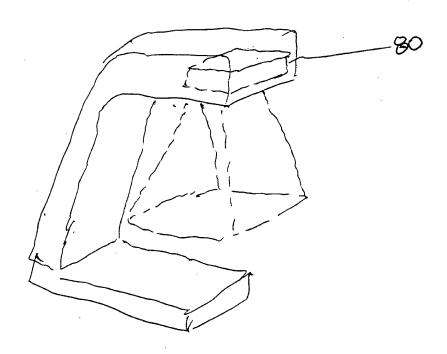




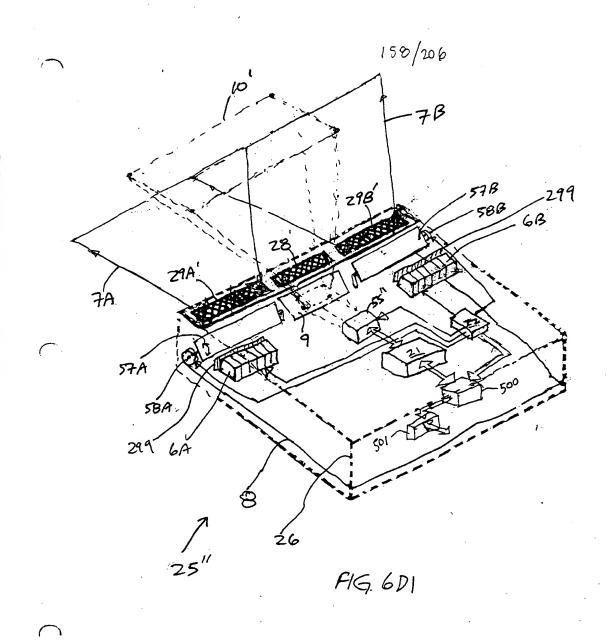


F/G. BCY

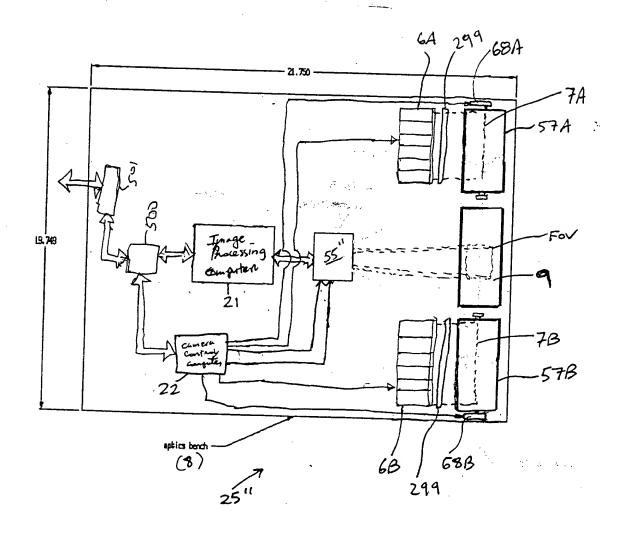
The contract of the contract o



F16:6C5

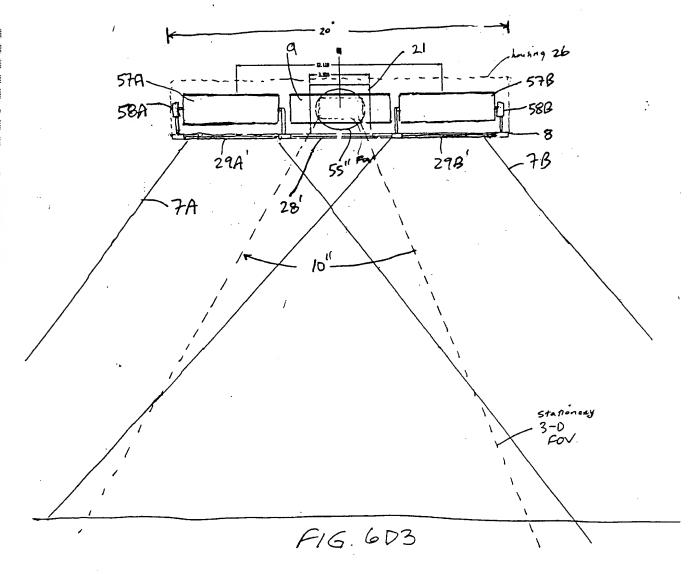


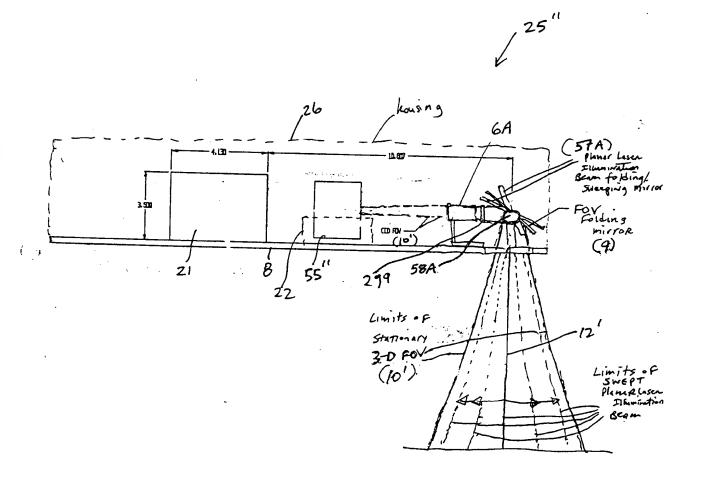
159/206



F1G.6DZ

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£16.6D4

variable FOV

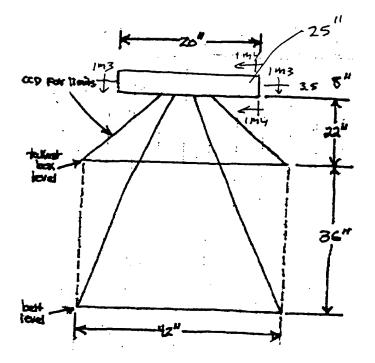
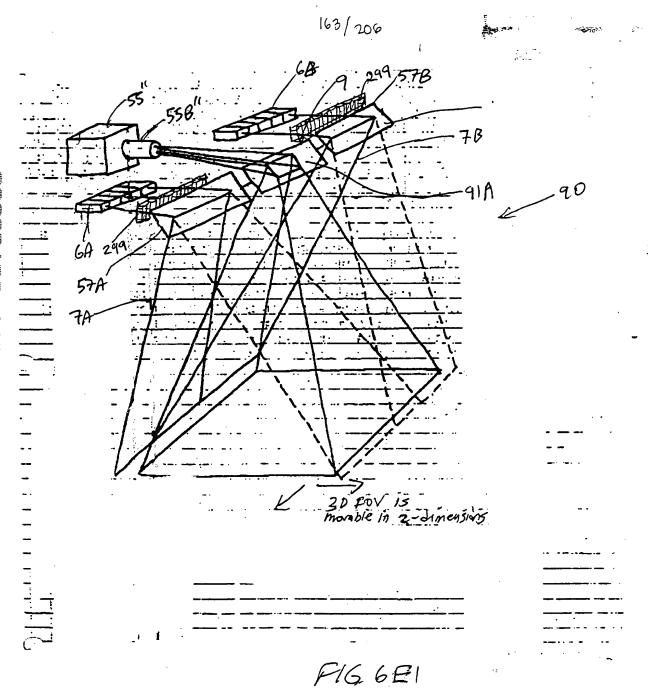
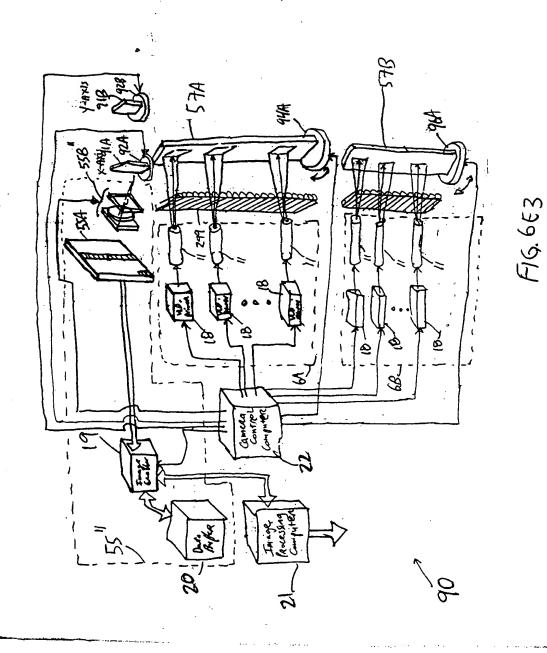


FIG. 6D5

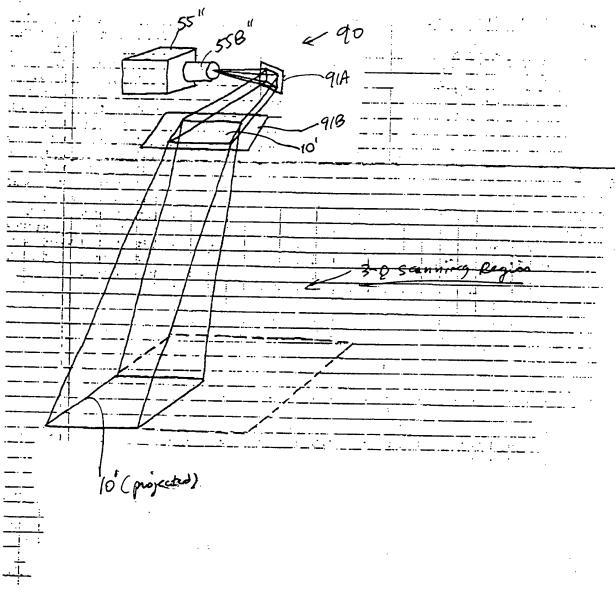


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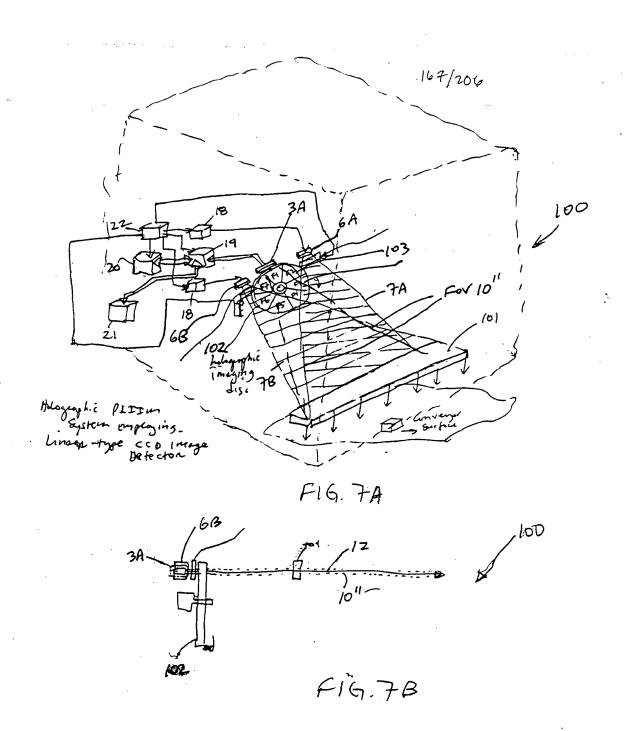
Ω

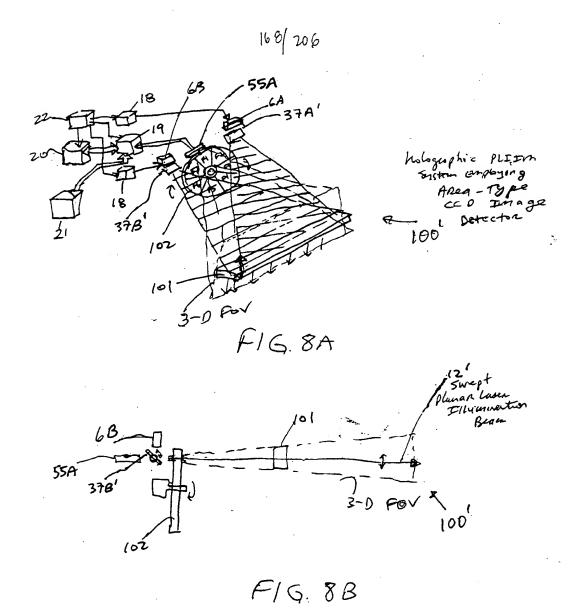


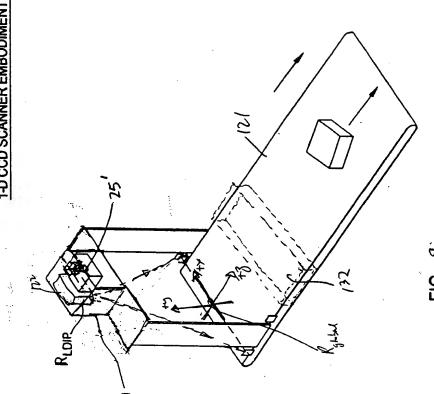


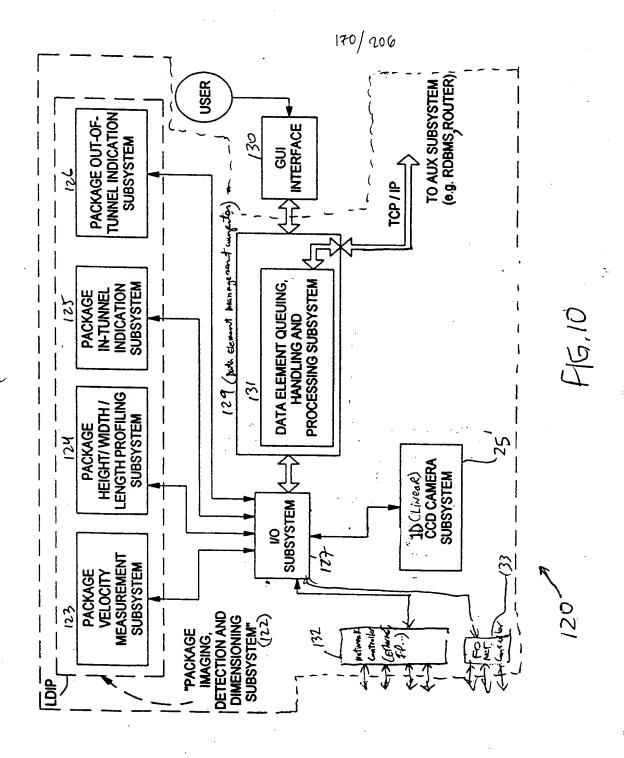


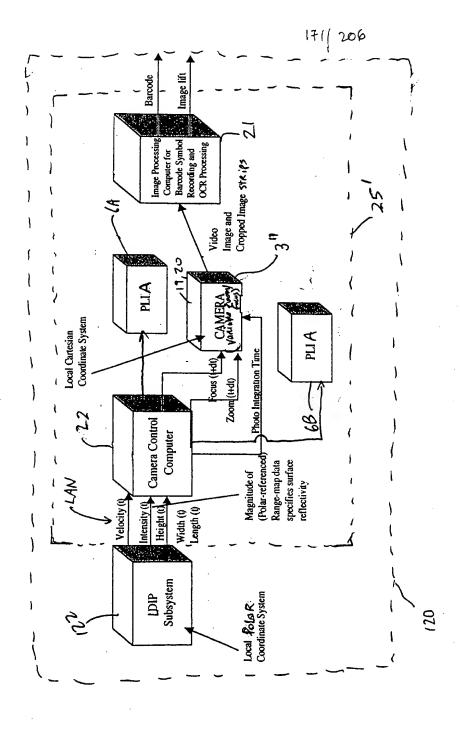
-- FIG 6E4



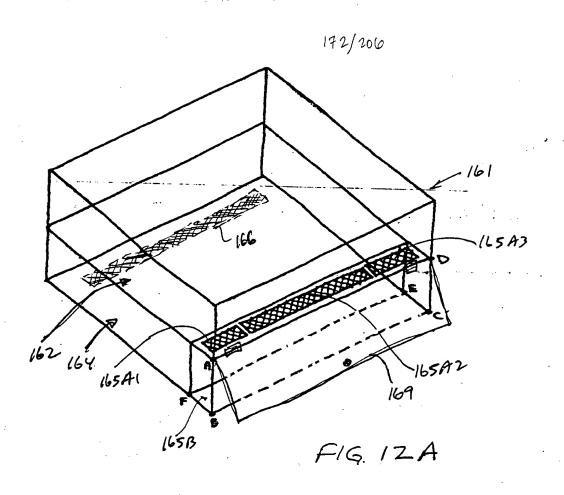


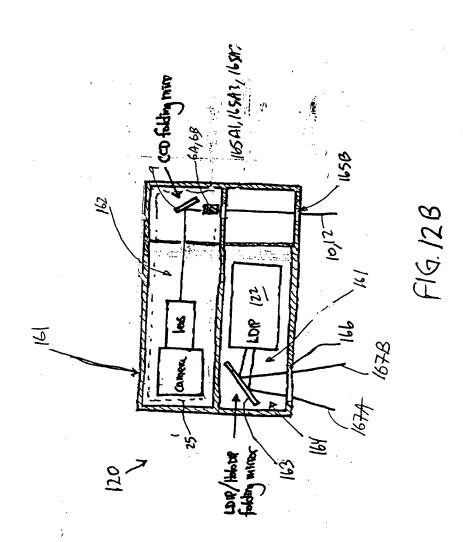






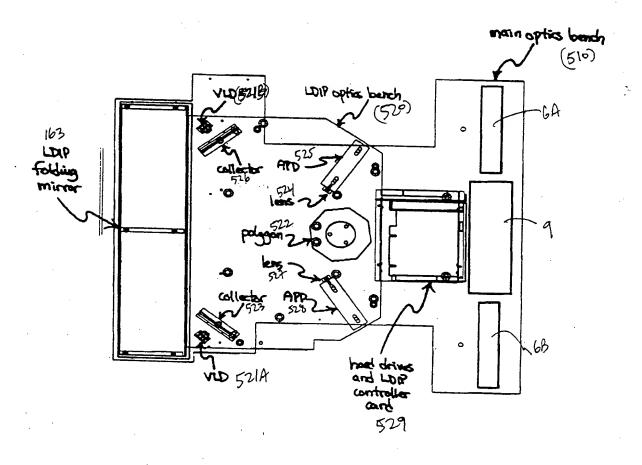
HG. 11





F16. 120

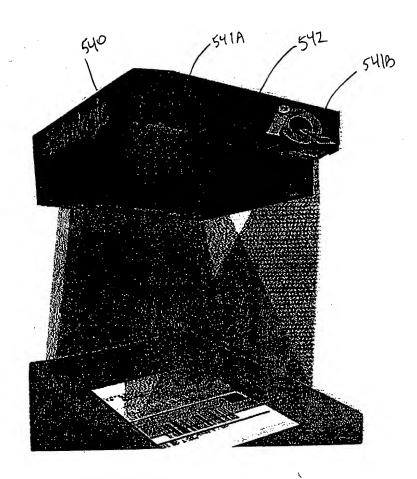
175/206



F1G 12D

F16.12E

(.main optics)



F1G. 13A



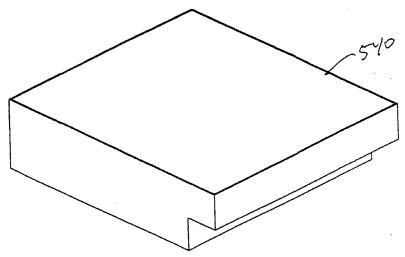
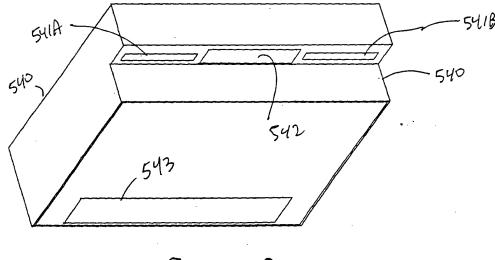


FIG. 13B



F16.13C

PLLIM-BASED PACKAGE IDENTIFICATION AND DIMENSIONING (PID) SYSTEM

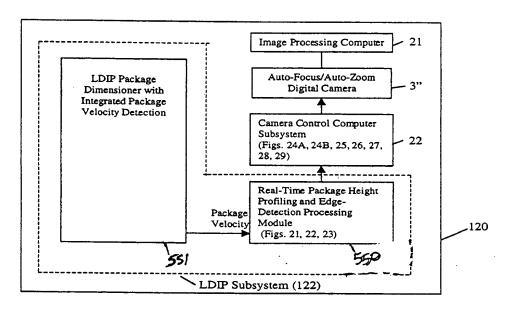
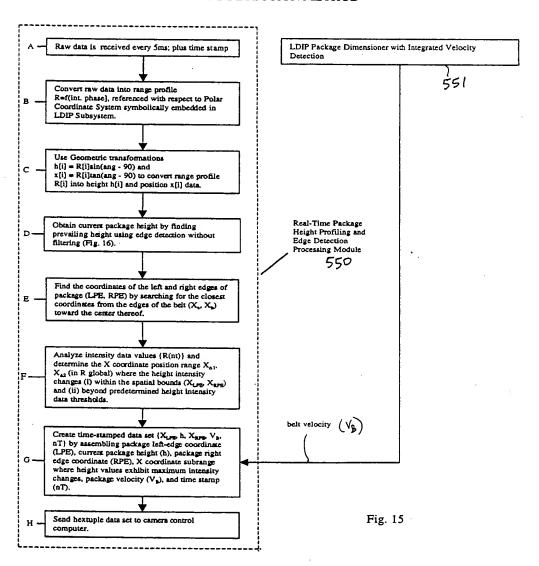


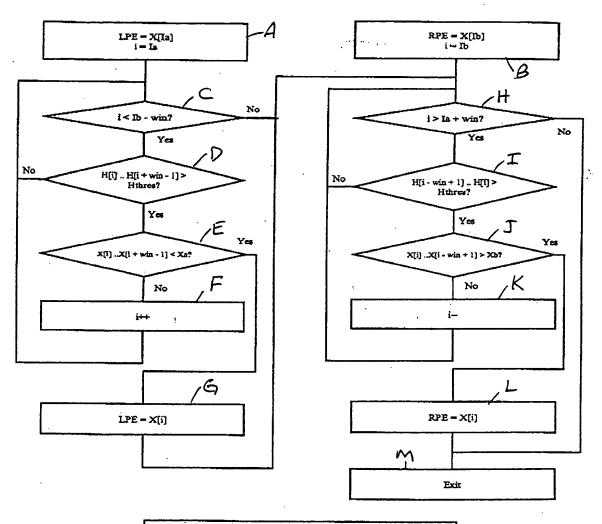
FIG. 14

LDIP REAL-TIME PACKAGE HEIGHT PROFILE AND EDGE DETECTION METHOD



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LDIP Real Time Package Edge Detection



Xa = location of belt left edge; Xb = location of belt right edge
Ia = belt edge edge pixel; Ib = belt right edge pixel
LPE = Left package edge; RPE = Right package edge
H[] = Pixel height array; X[] = Pixel location array
win = package detection window

F1G.16

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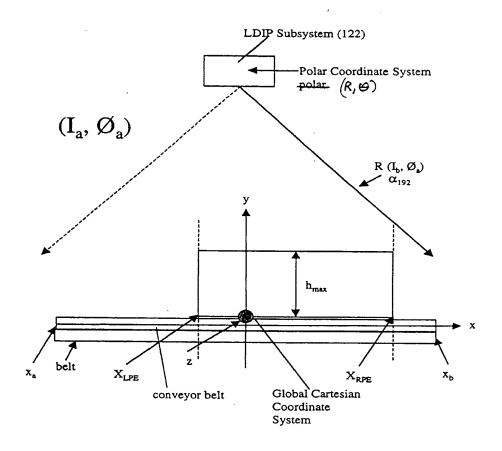


Fig. 17

45 A

H[]

Input height after

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INFORMATION MEASURED AT SCAN ANGLES BEFORE COORDINATE TRANSFORMS

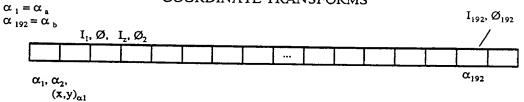


Fig. 17A

RANGE AND POLAR ANGLE MEASURES TAKEN AT SCAN ANGLE α BEFORE COORDINATE TRANSFORMS

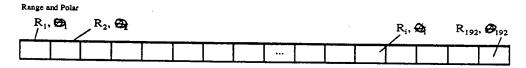
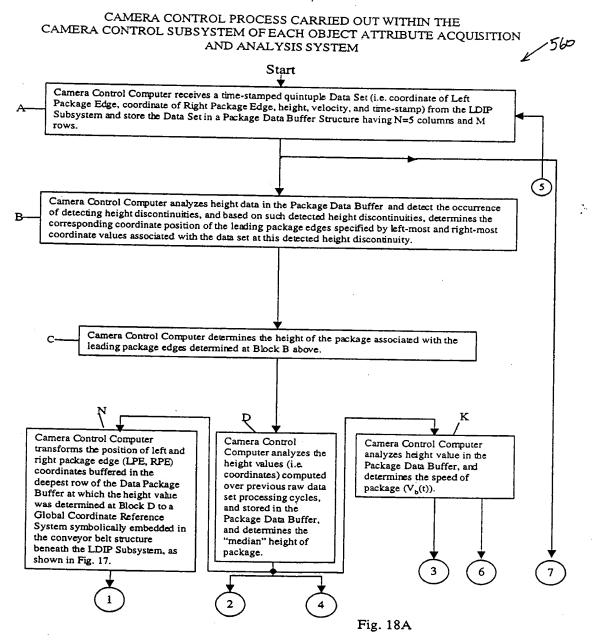
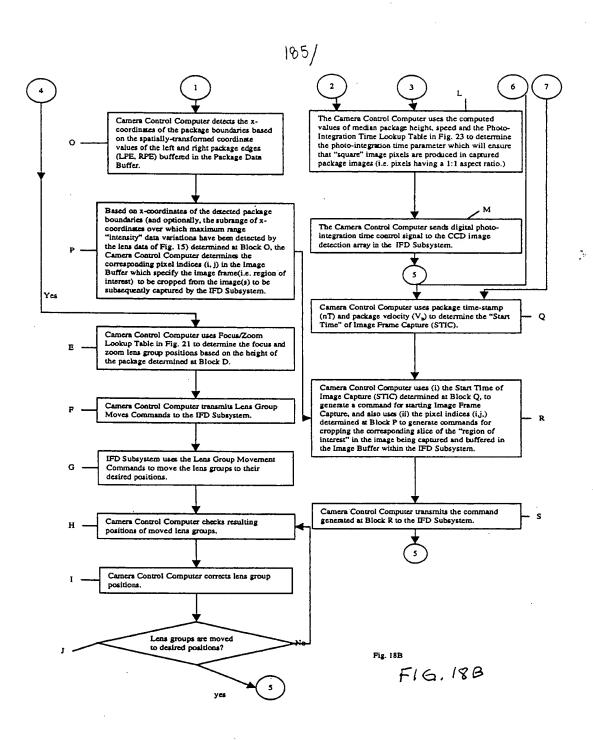


Fig. 17B

MEASURED PACKAGE HEIGHT AND POSITION VALUES AFTER COORDINATE TRANSFORMS

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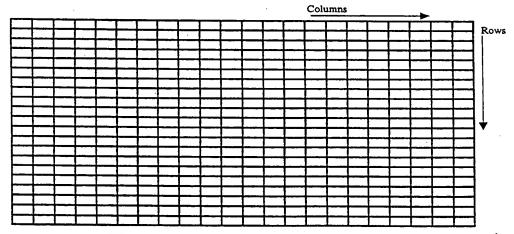


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x coordinate subrange where maximum range "intensity" variations have been detected

Left Package		Right Package		Package	Time-stamp	
Edge (LDE)	Package Helght (h)	Edge (RPE)	X	Velocity	(nT)	1
						Row
						Row :
						Row:
						Row
				1		Row
				1		1
				1		Row
ackage Da	ata Buffer (FIF	0)				7

Fig. 19



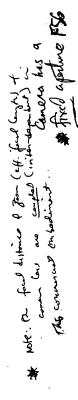
Camera Pixel Data Buffer pixel indices (i.j.)

Fig. 20

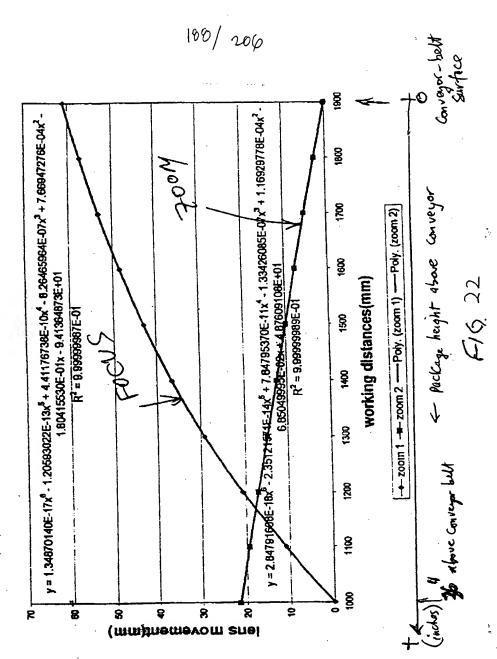
From and Fours lans Group position

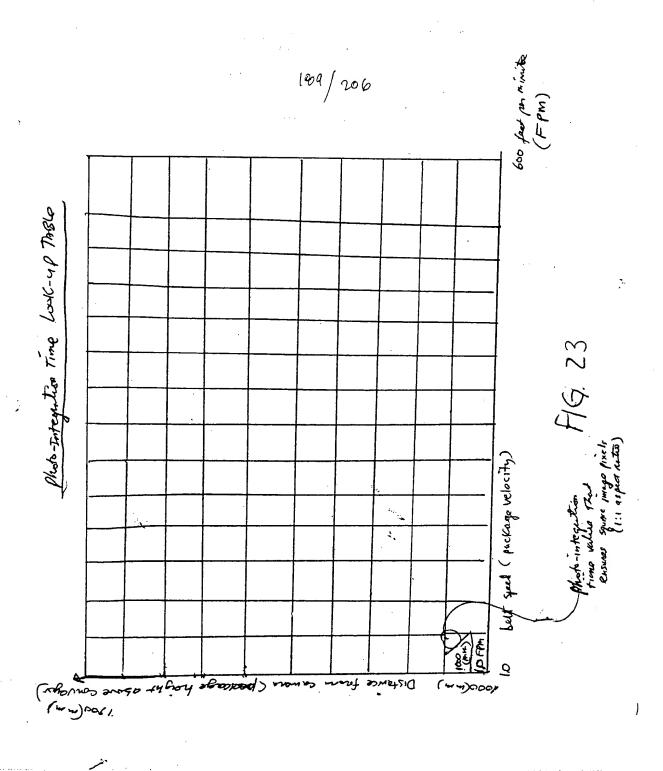
Focus group distance (mm) Y (Focus)	2.47E-05 10.99009783 20.65783177 29.10917002 36.47312595 42.87845436 48.4400338 53.25495831 57.40834303 60.98863615
Zoom group distance (mm) FY (Zoom)	21.57489228 19.38089696 17.10673434 (4.77137314 12.39153565 9.97914358 7.540639114 5.078194775 2.595989366 0.099972739
Distance from Camera Z	1000 (USE 1200 1100 1100 TECHNISHES 1500 Grances 1500 destances 1500 between 1154ed 1900 pants in table)

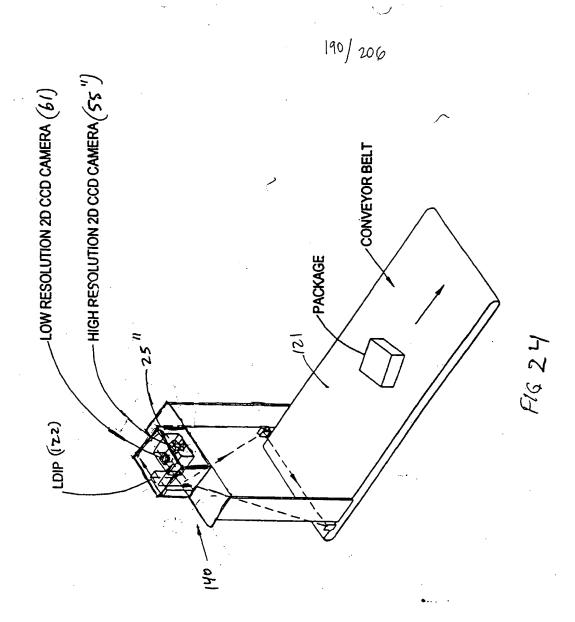
F16, 21

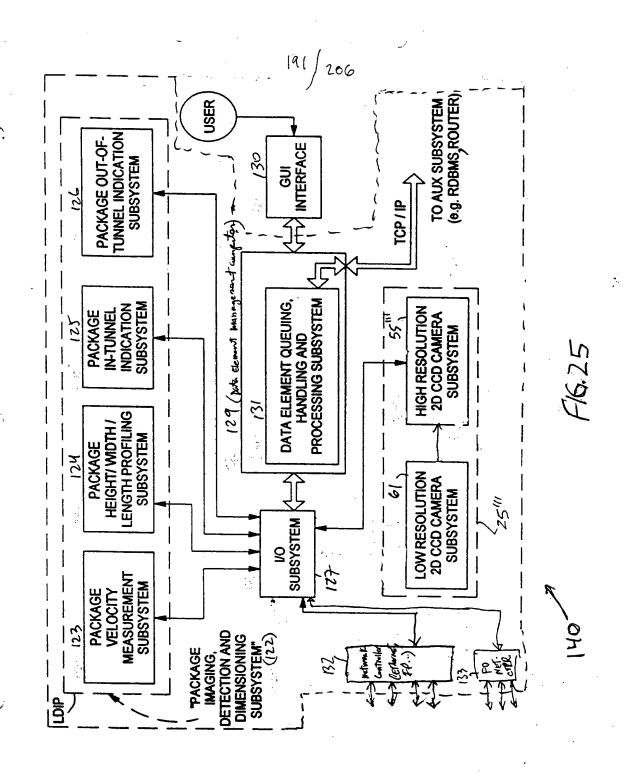


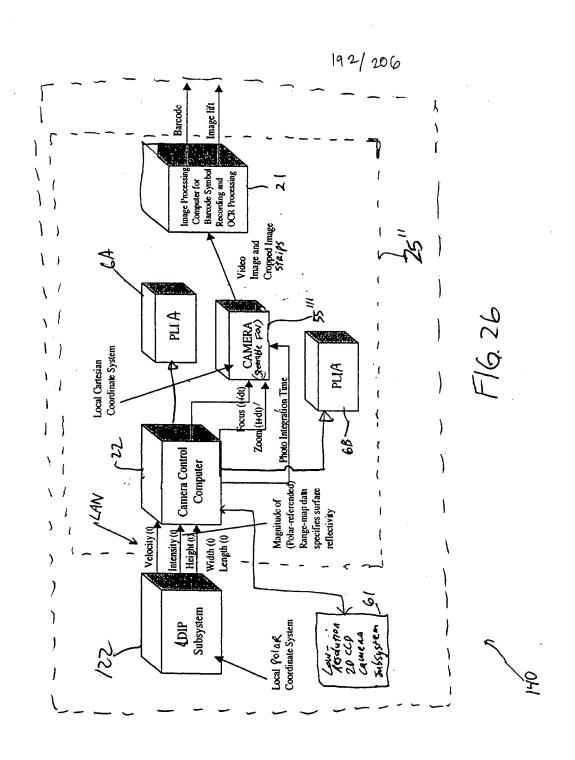
क्रिक्ट वासे 200ल lens movement vs. working distances



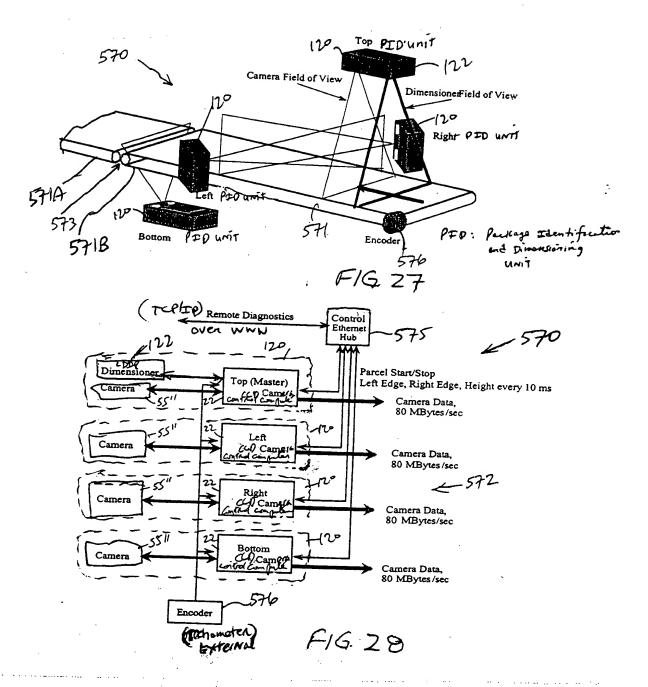




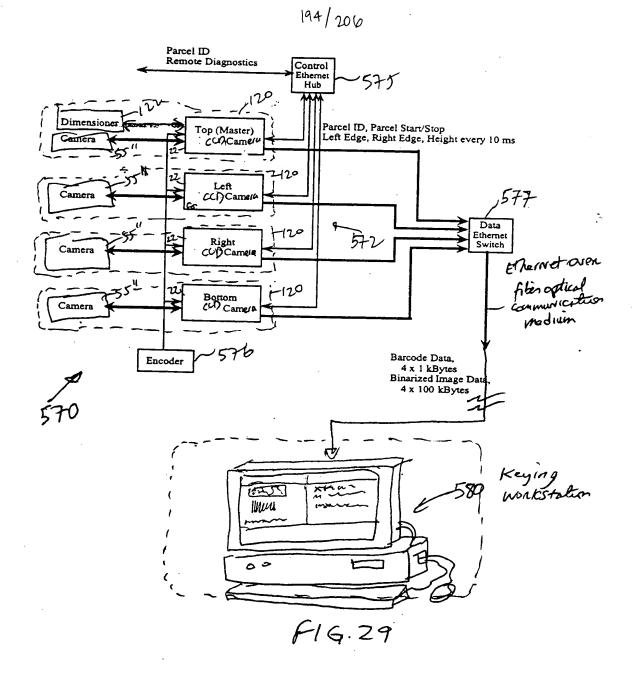


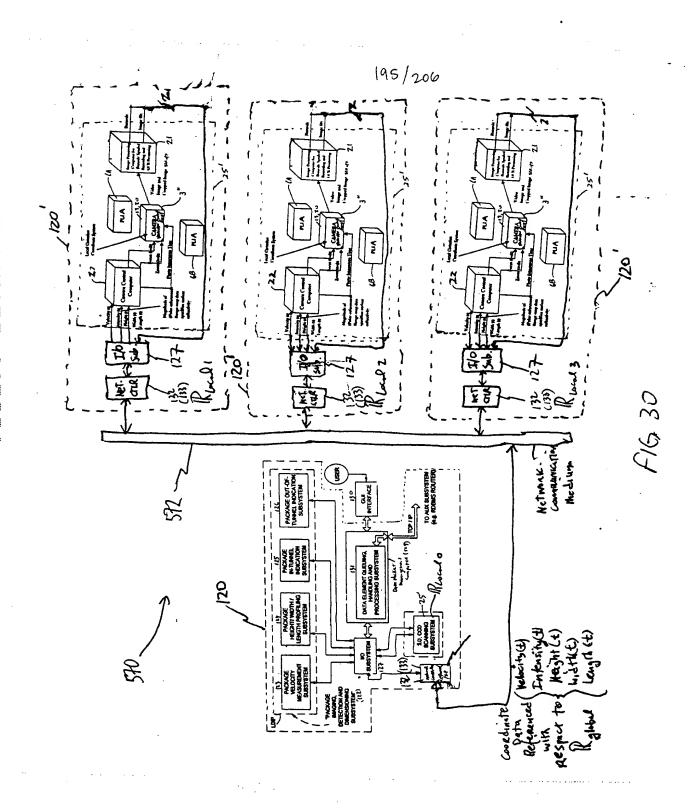


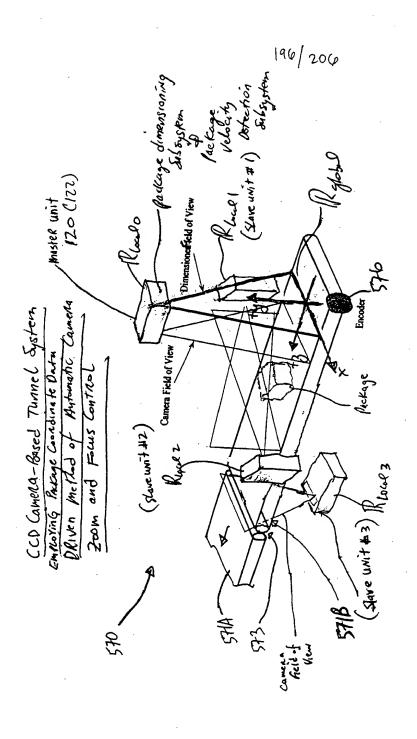
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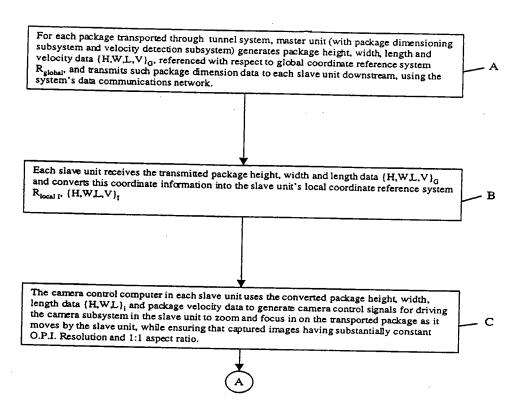




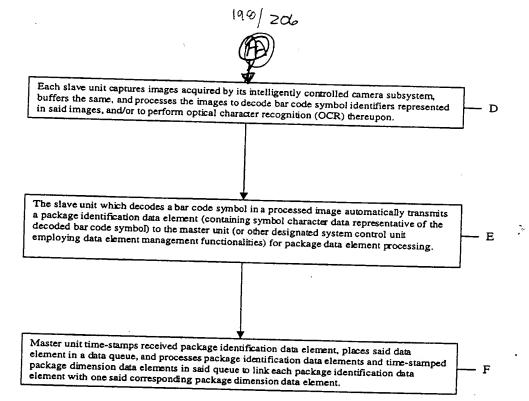
Parkuge Cooperinate Octa | 145 Puckuge Cooleanate Acta |

F16.31

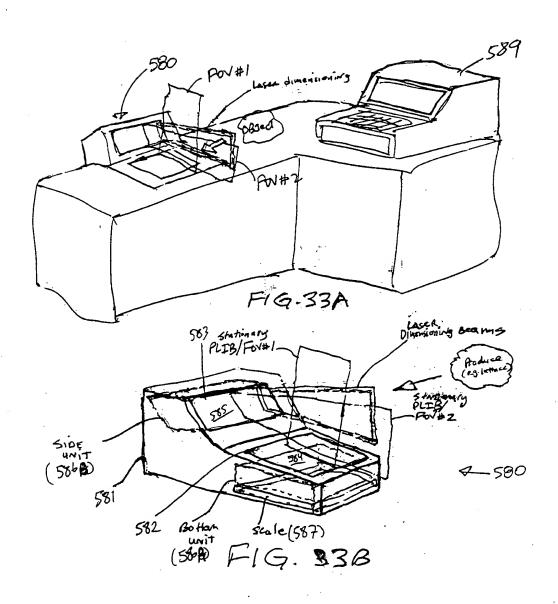


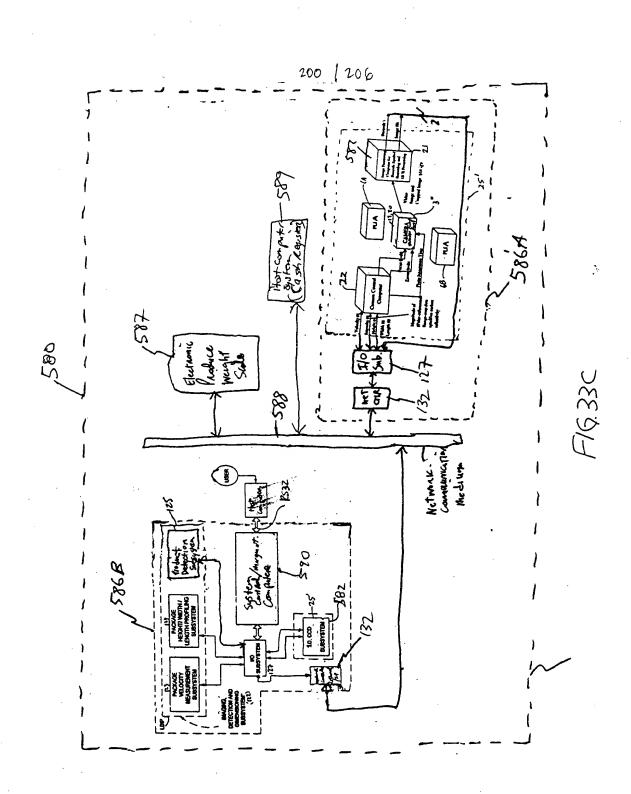


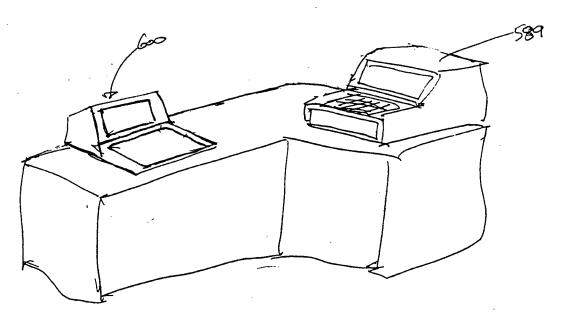




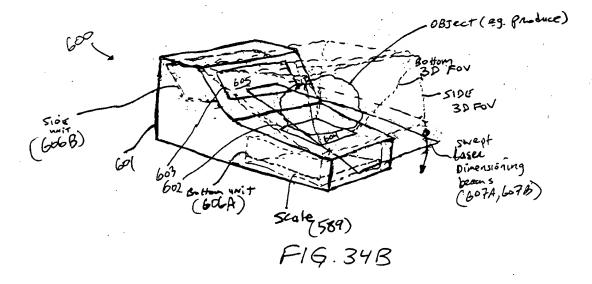


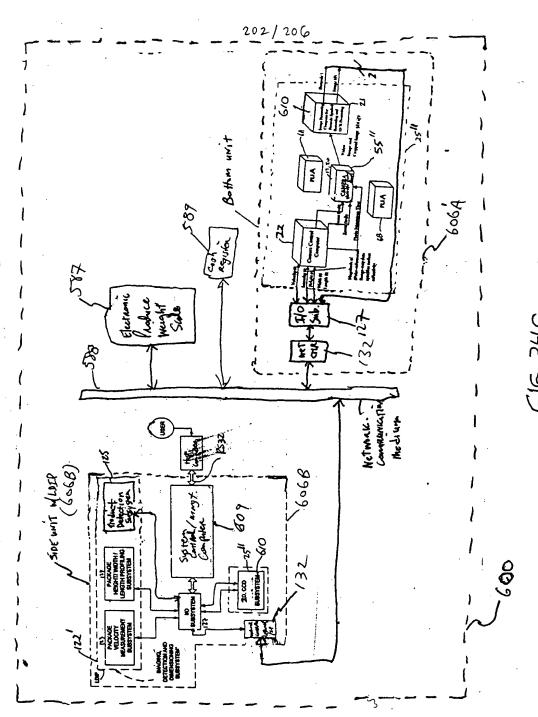




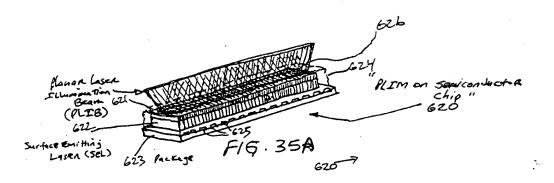


F1G. 34A

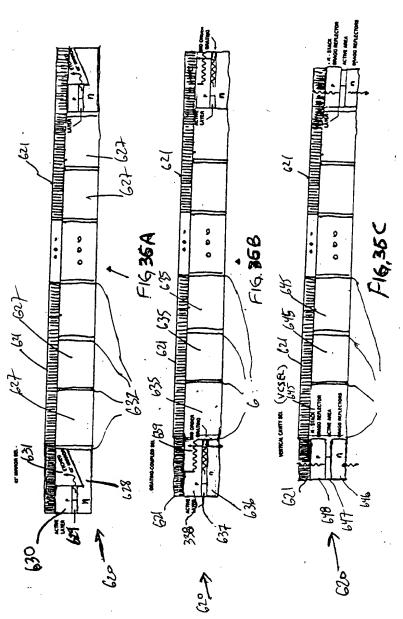


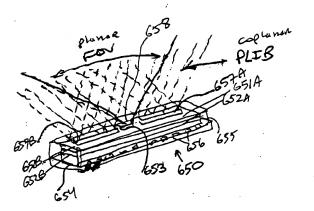


F19,34C

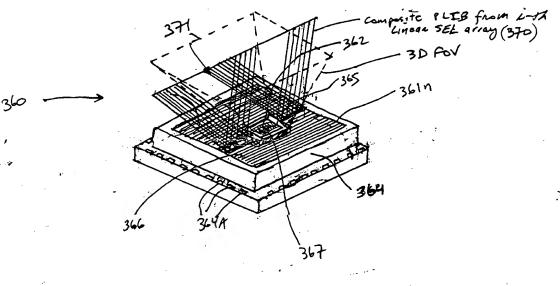




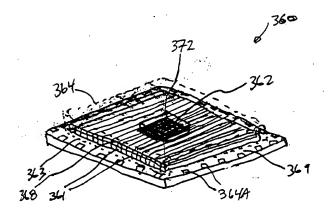




F1G. 37



F1G. 38 A



F16.38B